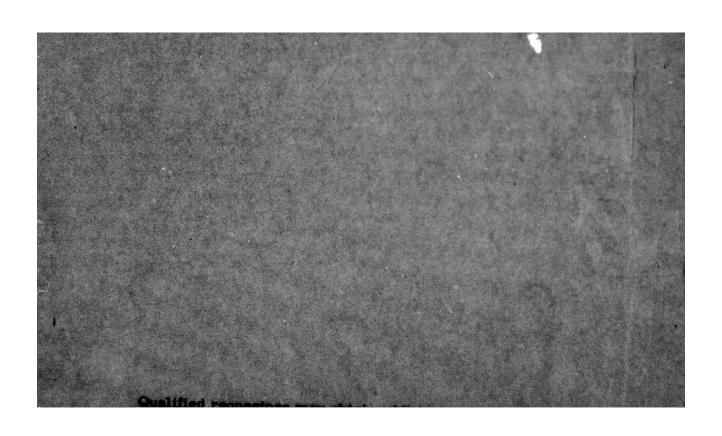


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SECURITY CLASSIFICATION OF THIS PAGE(When Date Entered) (10%) were found among all solutions. The computations by collocation were at least 30 times more time consuming than the integrations. In order to reduce the computation time in applying the former method for larger systems (such as 5deg anomalies), an alternative computation procedure is outlined.

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Foreword

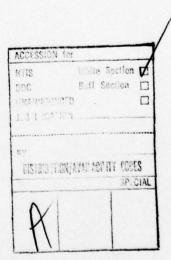
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1. Introduction

The gravity potential of the earth (W) can be decomposed into the gravitational potential (V) and the rotational potential (Φ):

$$W = V + \Phi$$

As V is harmonic outside the surface of the earth, it can be expanded into a series of spherical harmonics in this region (we assume that the series is convergent):

$$(1.1) V = \frac{GM}{r} \left\{ 1 + \sum_{n=2}^{\infty} \left(\frac{a}{r} \right)^n \sum_{m=0}^{n} \left(\overline{C}_{nm} \cos m \lambda + \overline{S}_{nm} \sin m \lambda \right) \overline{P}_{nm} (\sin \varphi) \right\}$$

where

G Newton's constant of gravitation

M mass of the earth

 (r, φ, λ) geocentric spherical coordinates of the computation point

Pna () normalized associated Legendre polynomial

c na, S na fully normalized spherical harmonic potential coefficients

a equatorial radius of the defined earth ellipsoid

In the study of the geopotential field it is most convenient to subtract a selected reference field:

$$U = \frac{GM}{r} \left\{ 1 + \hat{C}_{30} \left(\frac{a}{r} \right)^{2} \overline{P}_{20} \left(\sin \varphi \right) + \hat{C}_{40} \left(\frac{a}{r} \right)^{4} \overline{P}_{40} \left(\sin \varphi \right) \right\} + \Phi$$

where C_{20} and C_{40} are selected coefficients, from the potential W. The residual potential (T) is the so called disturbing potential:

(1.2)
$$T = W - U = \frac{GM}{a} \sum_{n=2}^{\infty} \left(\frac{a}{r}\right)^{n+1} \sum_{n=0}^{n} \left(\overline{C}_{nn} \cos m \lambda + \overline{S}_{nn} \sin m \lambda\right) \overline{P}_{nn} \left(\sin \varphi\right)$$

where

$$\overline{C}_{80} = \overline{C}_{20} - \hat{C}_{20}$$

$$\overline{C}_{40} = \overline{C}_{40} - \hat{C}_{40}$$

$$\overline{C}_{nm} = \overline{\overline{C}}_{nm}, \overline{S}_{nm} = \overline{\overline{S}}_{nm} \quad \text{for } (n,m) \neq (2,0) \text{ or } (4,0)$$

Now, by inserting (1.2) into the spherical approximation of "the fundamental boundary condition" (Heiskanen and Moritz, 1967, p. 88):

$$\Delta g = -\frac{\partial T}{\partial r} - \frac{2T}{r}$$

we obtain the gravity anomaly (Δg) in terms of the potential coefficients:

(1.3)
$$\Delta g = \gamma \sum_{n=2}^{\infty} (n-1) \sum_{m=0}^{n} (\overline{C}_{nm} \cos m \lambda + \overline{S}_{nm} \sin m \lambda) \left(\frac{a}{r}\right)^{n+2} \overline{P}_{nm} (\sin \varphi)$$

where

$$\gamma = GM/a^2$$

It is obvious from formula (1.1) that the coefficients $\overline{\overline{C}}_{nm}$ and $\overline{\overline{S}}_{nm}$ are dependent on the choice of a, but that $\overline{\overline{C}}_{nm}$ and $\overline{\overline{S}}_{nm}$ and are invariant quantities. On the other hand, for a fixed γ the gravity anomaly in (1.3) is independent of the choice of a, whenever:

$$\overline{C}_{nm} a^{n+2}$$
 and $\overline{S}_{nm} a^{n+2}$

are invariant. This means that for two different a-values (a_1, a_2) and $\gamma = constant$ the gravity anomalies in (1.3) are the same, if (with obvious notations):

(1.4)
$$\left\{\frac{\overline{C}_{nn}}{\overline{S}_{nn}}\right\}_{a_1} = \left(\frac{a_2}{\overline{a_1}}\right)^{n+2} \left\{\frac{\overline{C}_{nn}}{\overline{S}_{nn}}\right\}_{a_2}$$

This relation will be useful in the following application of estimating the coefficients $\overline{C}_{n\,m}$ and \overline{S}_{nm} .

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2. Covariance Functions

Suppose that the gravity field is harmonic, homogeneous and isotropic. Then the spatial covariance function of the point free-air gravity anomalies Δg_1 and Δg_1 is given by (Moritz, 1972, p. 89):

(2.1)
$$c_{ij} = cov (\Delta g_i, \Delta g_j) = \sum_{n=2}^{\infty} c_n s^{n+2} P_n (cos \psi_{ij})$$

where

 $s = r_8^2/r_1 r_j$ $r_8 = radius$ of the Bjerhammar sphere $r_k = r_m + h_k$, k = i, j $r_m = radius$ of mean sea level h_1 , $h_j =$ elevations of points P_1 and P_j $c_m =$ degree variances of Δg

The corresponding covariance function of the mean gravity anomalies $\Delta \bar{g}_i$ and $\Delta \bar{g}_j$, where:

$$\overline{\Delta g}_k = \frac{1}{\Delta \sigma_k} \iint_{\Delta \sigma_k} \Delta g \, d\sigma ; \quad k = i, j$$

is given by

(2.2)
$$\overline{\overline{c}}_{ij} = \operatorname{cov}(\Delta \overline{g}_{i}, \Delta \overline{g}_{j}) = \frac{1}{\Delta \sigma_{i} \Delta \sigma_{j}} \iint_{\Delta \sigma_{i}} \int_{\Delta \sigma_{j}} e_{ij} d\sigma d\sigma$$

In the same way we obtain the following cross-covariance function between Δg_i and $\overline{\Delta g}_j$:

(2.3)
$$\overline{c}_{ij} = \frac{1}{\Delta \sigma_j} \iint_{\Delta \sigma_j} c_{ij} d\sigma$$

In these formulae $\Delta \sigma$ is a part of the unit sphere σ . For small regions $\Delta \sigma_1$ and $\Delta \sigma_2$ we may, without loss of significance, assume that r_1 and r_2 are constants. Then (2.2) and (2.3) become:

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(2.2')
$$\overline{\overline{c}}_{ij} = \sum_{n=2}^{\infty} c_n s^{n+2} \frac{1}{\Delta \sigma_i \Delta \sigma_j} \iiint_{\Delta \sigma_i \Delta \sigma_j} P_n (\cos \psi_{ij}) d\sigma d\sigma$$

The common way to determine the spherical harmonic coefficients of the earth's gravity field from terrestrial data is by means of integration of mean gravity anomalies over a mean earth sphere. See for example Rapp (1977a). Due to the orthogonal functions the coefficients are obtained directly in the integrations. Rigorously, it is required that the gravity anomalies are located on the sphere of integration, but in reality, due to the variation of the elevation of the terrain, this is not the case. This terrain deviation can be corrected for by adding the Molodenshy G_1 term to the mean anomalies. Pellinen (1962) has indicated that the neglect of this term can cause errors in the low degree coefficients of 10 to 20 percent. Numerical results of Rapp (1977a) agree with this error estimate, but the results were based on a number of assumptions relating the G_1 term to the terrain correction.

In practice, the computation of the Molodenshy correction term for the terrain may be very difficult and laborious, especially in areas with rapidly varying topography. It is therefore of interest to find a technique for the determination of the potential coefficients that does not include the computation of the G_1 terms, yet retains the rigor of that procedure. One such method was given by Rapp (1977b), where least-squares collocation was used for an upward continuation of the terrestrial mean anomalies to a bounding sphere. Once the anomalies are given at the sphere the integration can be applied strictly for the determination of the potential coefficients. Rapp (1977b) found that the neglect of G_1 caused errors less than 7.5% for harmonics up to degree 40.

In the present study the idea is to estimate the potential coefficients directly by applying least-squares collocation to the terrestrial mean gravity anomalies. The integration is then taken care of in the cross-covariance matrix. The advantage of using such a method is that the terrain correction is easily included and that the various accuracies of the mean anomalies can be taken into account, which is not obvious in the integration approach.

In collocation a physical quantity V may be predicted from a vector of (mean) gravity anomalies Δg by the relation:

(1.5)
$$V = c_V^T (G + D)^{-1} \Delta g$$

where

 $c_v^{\dagger} = cross-covariance matrix (V, \Delta g)$

 $C = auto-covariance matrix (\Delta g, \Delta g)$

D = error covariance matrix

The prediction errors are estimated by

(1.6)
$$m_v^2 = C_0 - c_v^{\dagger} (C + D)^{-1} c_v$$

Where Co is the variance of V prior to prediction. For further details on these basic formulae see Moritz (1972).

The collocation technique requires that the relevant covariance functions are known. In the next section we are going to study these functions for the present application.

and

(2.3')
$$\overline{c}_{ij} = \sum_{n=2}^{\infty} c_n \, s^{n+2} \, \frac{1}{\Delta \sigma_j} \, \iint_{\Delta \sigma_j} P_n \left(\cos \psi_{ij}\right) \, d\sigma$$

Formulae (2.2') and (2.3') are very laborious to compute in practice due to the many numerical integrations. Approximate mean covariance functions may be obtained by using the β_n function of Meissl (1971, p. 23):

$$\beta_{n} = \frac{1}{1 - \cos \psi_{0}} \frac{1}{2n+1} [P_{n-1}(\cos \psi_{0}) - P_{n+1}(\cos \psi_{0})]$$

where ψ_0 is the radius of a circular cap of area equal to the relevant block size of the mean anomalies. Then, the above covariance functions become (approximately) (cf. Figure 2 a-b):

(2.2')
$$\overline{\overline{c}}_{ij} = \sum_{n=2}^{\infty} c_n s^{n+2} \beta_n^2 P_n (\cos \psi_{ij})$$

and

(2.3")
$$\overline{\mathbf{c}}_{ij} = \sum_{n=2}^{\infty} \mathbf{c}_n \, \mathbf{s}^{n+2} \, \boldsymbol{\beta}_n \, \mathbf{P}_n \, (\cos \psi_{ij})$$

As

$$\beta_n \to 0$$
 as $n \to \infty$

it is usually sufficient to truncate the series (2.2") and (2.3") at a few hundred degrees (dependent upon the block size) without loss of significance.

We also give the autocovariance relations between the potential coefficients. In Moritz (1970) the relations are given for the anomaly coefficients $(\overline{a}_{nm}, \overline{b}_{nm})$. As \overline{a}_{nm} and \overline{b}_{nm} are related to the potential coefficients \overline{C}_{nm} and \overline{S}_{nm} according to:

$$\left\{ \frac{\overline{C}_{nm}}{\overline{S}_{nm}} \right\} = \frac{1}{\gamma (n-1)} \, \left\{ \frac{\overline{a}_{nm}}{\overline{b}_{nm}} \right\}$$

where γ is the mean gravity at sea-level, we obtain from Moritz (ibid.):

(2.4)
$$\operatorname{cov}(\overline{C}_{nm}, \overline{C}_{pq}) = \operatorname{cov}(\overline{S}_{nm}, \overline{S}_{pq}) = \frac{c_n}{(2n+1)(n-1)^2 \gamma^2} \delta_{np} \delta_{mq}$$

where

$$\delta_{np} = \begin{cases} 1 & \text{if } n = p \\ 0 & \text{if } n \neq p \end{cases}$$

and

$$\operatorname{cov}(\overline{C}_{nm}, \overline{S}_{pq}) = 0$$
 in any case.

The above covariance relations will be useful in our application a collocation.

Finally, we like to mention that the mean covariance functions (2.2) and (2.3) can in addition, be approximated by the corresponding point covariance functions simply by increasing the radii r_1 and r_2 by a feasible constant. This type of smoothed covariance functions was discussed in Tscherning and Rapp (1974, Section 10) and Schwarz (1976, Section 7).

3. Application of Collocation

We assume that the external gravity field of the earth may be expanded into a series of spherical harmonics at a sphere of radius R. Then we have [cf. (1.3)]:

(3.1a)
$$\Delta \mathbf{g}_{R} = \gamma \sum_{n=2}^{\infty} (n-1) \left(\frac{\mathbf{r}_{B}}{R}\right)^{n+2} \sum_{n=0}^{n} (\overline{\mathbf{C}}_{nm} \cos m \lambda + \overline{\mathbf{S}}_{nm} \sin m \lambda) \overline{\mathbf{P}}_{nm} (\sin \varphi)$$

where

$$\gamma = GM/a^2$$
 $r_B = radius of the Bjerhammar sphere$

and

(3.1b)
$$\left\{\frac{\overline{C}_{nm}}{\overline{S}_{nm}}\right\}_{r_B} = \frac{1}{4\pi\gamma(n-1)(r_B/R)^{n+2}} \iint_{\sigma} \Delta g_R \overline{P}_{nm} (\sin \varphi) \left\{\frac{\cos m\lambda}{\sin m\lambda}\right\} d\sigma$$

Formula (3.1b) is the basic equation we are going to use for estimating the potential coefficients. The coefficients determined by (3.1b) are independent of the choice of R. Thus by choosing R as the radius of the Brioullin sphere (bounding all the mass of the earth) we have a theoretically most attractive situation, because the series expansion (3.1a) is rigorously convergent at this sphere (cf. Sjöberg, 1977). The

standard representation of the coefficients \overline{C}_{nn} and \overline{S}_{nn} in the literature is with reference to the equatorial radius of the earth (a) (and not to the Bjerhammar sphere as in (3.1b)). The conversion from (3.1b) to this representation was given in (1.4):

(3.2)
$$\left\{\frac{\overline{C}_{nn}}{\overline{S}_{nn}}\right\}_{a} = \left(\frac{\mathbf{r}_{\theta}}{\overline{a}}\right)^{n+2} \left\{\frac{\overline{C}_{nn}}{\overline{S}_{nn}}\right\}_{\mathbf{r}_{\theta}}$$

Theoretically, the point gravity anomaly Δg_R in (3.1a) can be estimated from a vector of mean gravity anomalies by means of formula (1.5):

$$\Delta \mathbf{g}_{R} = \mathbf{c}_{R}^{T} (C + \mathbf{D})^{-1} \Delta \mathbf{g}$$

where

$$c_R^{\dagger} = cross-covariance matrix (\Delta g, \Delta g)$$

The element $(c_R^{\dagger})_{i,j}$ is given by (2.3') with $r_i = R$ and $C_{i,j}$ is given by (2.2'). The error covariance matrix D can be estimated by the diagonal matrix formed by the a priori estimated mean anomaly variances.

By inserting (3.3) into (3.1b) we arrive at:

(3.4)
$$\left\{\frac{\overline{C}_{nm}}{\overline{S}_{nm}}\right\} = \left\{\frac{c_{c}}{c_{s}}^{T}\right\} (C + D)^{-1} \underline{\Delta}g$$

where the elements of cc and cs become:

(3.5)
$$\left\{ \begin{pmatrix} (c_{c})_{ij} \\ (c_{s})_{ij} \end{pmatrix} = \frac{1}{4\pi\gamma(n-1)(r_{s}/R)^{n+2}} \iint_{\sigma} \overline{c}_{ij} \overline{P}_{nm} (\sin \varphi) \left\{ \begin{pmatrix} \cos m\lambda \\ \sin m\lambda \end{pmatrix} d\sigma \right\}$$

We are going to simplify (3.5) by taking into account the orthogonality of the spherical harmonics (Heiskanen and Moritz, 1967, p. 29). Using the notations:

$$\left\{ \frac{\overline{R}_{nu} (\varphi, \lambda)}{\overline{S}_{nu} (\varphi, \lambda)} \right\} = \overline{P}_{nu} (\sin \varphi) \left\{ \frac{\cos m \lambda}{\sin m \lambda} \right\}$$

we obtain from (2.3'):

$$(3.6) \qquad \frac{1}{4\pi} \iint \overline{\mathbf{c}}_{ij} \ \overline{\mathbf{R}}_{nn} (\varphi, \lambda) \ d\sigma = \frac{1}{\Delta \sigma_j} \iint_{\Delta \sigma_j} \sum_{n=2}^{\infty} \mathbf{c}_n \ \mathbf{s}^{n+2} \ \frac{1}{4\pi} \iint \mathbf{P}_n (\cos \psi_{ij}) \ \overline{\mathbf{R}}_{nx} (\varphi, \lambda) \ d\sigma \ d\sigma$$

$$= \frac{c_n}{2n+1} s^{n+2} \frac{1}{\Delta \sigma_j} \iint_{\Delta \sigma_j} \overline{R}_{nm} (\varphi, \lambda) d\sigma$$

A completely analogous result is obtained for \overline{S}_{nn} . Inserting the result of (3.6) into (3.5) we finally obtain:

(3.7)
$$\left\{ \frac{(c_{c})_{ij}}{(c_{s})_{ij}} \right\} = \frac{c_{n}}{\gamma(2n+1)(n-1)} \left(\frac{r_{s}}{r_{j}} \right)^{n+2} \frac{1}{\Delta \sigma_{j}} \iint_{\Delta \sigma_{j}} \overline{P}_{nm}(\sin \varphi) \left\{ \frac{\cos m \lambda}{\sin m \lambda} \right\} d\sigma$$

where

$$\frac{1}{\Delta\sigma_{j}}\iint_{\Delta\sigma_{j}} \overline{P}_{nn} (\sin\varphi) \left\{ \frac{\cos m\lambda}{\sin m\lambda} \right\} d\sigma =$$

$$= \frac{1}{\sin\varphi_{\text{N}} - \sin\varphi_{\text{S}}} \int_{\varphi_{\text{S}}}^{\varphi_{\text{N}}} \overline{P}_{\text{nm}} \left(\sin\varphi\right) \cos\varphi \, d\varphi \quad x \left\{ \begin{array}{ll} 1 & \text{if } \cos m\lambda \text{ with } m = 0 \\ (\sin m\lambda_{\varepsilon} - \sin m\lambda_{\text{W}})/m \text{ if } \cos m\lambda \\ & \text{with } m \neq 0 \\ (\cos m\lambda_{\text{W}} - \cos m\lambda_{\varepsilon})/m \text{ if } \sin m\lambda \\ & \text{with } m \neq 0 \\ 0 & \text{if } \sin m\lambda \text{ with } m = 0 \end{array} \right.$$

 φ_s , φ_N , λ_E , λ_W = geocentric latitudes and longitudes of the corners of the block $\Delta \sigma_1$

If \overline{c}_{ij} is approximated by (2.3") the formula analogous to (3.7) becomes:

$$(3.7') \left\{ \frac{(c_{c})_{ij}}{(c_{s})_{ij}} \right\} = \frac{c_{n} \beta_{n}}{\gamma (2n+1)(n-1)} \left(\frac{r_{B}}{r_{j}} \right)^{n+2} \overline{P}_{nB} \left(\sin \overline{\varphi} \right) \left\{ \frac{\cos m \overline{\lambda}}{\sin m \overline{\lambda}} \right\}$$

where

$$\overline{\varphi} = (\varphi_N + \varphi_S)/2$$

$$\overline{\lambda} = (\lambda_E + \lambda_W)/2 \qquad -8$$

4. Error Analysis

Suppose that the gravity anomaly Δg_1 used in formula (3.1b) has the error ϵ_1 . The error propagation to \overline{C}_{nm} is accordingly:

$$d\,\overline{C}_{na} = \frac{1}{4\pi\,\gamma (n-1)(r_B/R)^{n+2}} \iint_{\sigma} \epsilon_i \,\overline{R}_{na} (\varphi,\lambda) \,d\,\sigma$$

and the mean square error of C nm becomes:

$$(4.1) \quad \overline{\mathbf{m}}_{c_{nm}}^{2} = \mathbf{M} \left\{ d\overline{\mathbf{C}}_{nm} \right\} =$$

$$= \left\{ \frac{1}{\gamma (\mathbf{n} - 1) (\mathbf{r}_{B} / R)^{n+2}} \right\}^{2} \mathbf{M}_{i} \left\{ \mathbf{M}_{j} \left\{ \sigma_{ij} \overline{\mathbf{R}}_{nm} (\boldsymbol{\varphi}_{i}, \lambda_{i}) \overline{\mathbf{R}}_{nm} (\boldsymbol{\varphi}_{j}, \lambda_{j}) \right\} \right\}$$

where

$$\sigma_{ij} = M \{ \epsilon_i \epsilon_j \} = \frac{1}{4\pi} \iint \epsilon_i \epsilon_j d\sigma$$

$$\psi_{ij} = \text{const.}$$

and

$$M_{i} = \frac{1}{4\pi} \iint_{\mathbf{\sigma}} d\mathbf{\sigma}_{i}$$

As Δg of formula (3.1b) is estimated by means of collocation, σ_{ij} is the prediction covariance of that method. Moritz (1972), formula (3-39) with A=0 gives

(4.2)
$$\sigma_{ij} = C_{ij} - \overline{C}_i^{\dagger} (C + D)^{-1} \overline{C}_j$$

where the covariances of the right member are those defined in (3.3). Inserting (4.2) into (4.1) and carrying out the integrations, we finally obtain:

(4.3a)
$$\overline{m}_{c_{nn}}^{2} = \frac{c_{n}}{(2n+1)(n-1)^{2}\gamma^{2}} - c_{c}^{\dagger} (C+D)^{-1} c_{c}$$

where the elements of c_c are given by (3.7). In the same way we obtain the mean square error for \overline{S}_{nn} :

(4.3b)
$$\overline{m}_{s_{nn}}^{2} = \frac{c_{n}}{(2n+1)(n-1)^{2} \gamma^{2}} - c_{s}^{T} (C+D)^{-1} c_{s}$$

We notice that (4.3a-b) give exactly the error estimates we would expect in collocation with the prediction formula (3.4). Cf. formulae (1.5) and (1.6).

5. Computations

A global coverage of 416 10° equal area free air gravity anomalies were available as input data. (These anomalies had been derived using the data of Rapp (1977a) and the methods described by Hajela (1975).) In all compute 1 covariance functions the degree variances implied by the subroutine COVA. Tscherning and Rapp (1974) were used with $c_2 = 7.5 \text{ mgal}^2$. The cross-covariance functions were computed by numerical integration according to formula (3.7) [derived from (2.3)]. However, for the auto-covariance function we felt that it was unreasonable to use the corresponding, very laborious formula (2.2). Instead, we tried two different approximate formulae. In order to save computer time the auto-covariance function for the mean anomalies for zero-elevations ($h_1 = h_3 = 0$) was stored in a table and the current values were interpolated among the tabulated values. When elevation information was included in the process the table was used only to determine the auto-covariances between ocean-block mean anomalies.

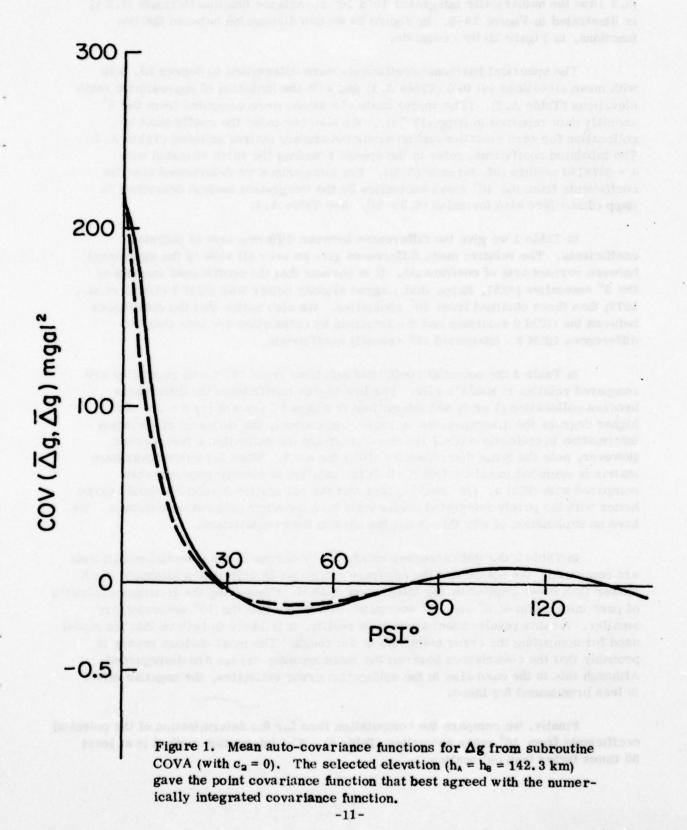
The following reference data were anticipated:

a = 6378140 m $\overline{C}_{20} = -484.198 \times 10^{-6}$ $\overline{C}_{40} = 0.790333 \times 10^{-6}$ f = 1/298.247

In a first test of the prediction formulae (3.4) and (4.3 a-b), the autocovariance function was approximated by the corresponding point covariance function at the best fitting elevation $(h_1 = h_1 = 142.3 \text{ km})$, cf. the end of section 2). Figure 1 indicates a fair agreement between this covariance function and the one implied by a numerical integration of the point covariance function over $10^{\circ} \times 10^{\circ}$ blocks (around the equator). However, the prediction result was poor and especially the error estimates were useless (because of negative variances!). It was apparent from the test that choice of mean covariance function was very critical, especially for the outcome of the prediction errors.

Second, the auto-covariance function was computed according to formula (2.3). It was found that the series could be accepted when truncated at degree 200 (except for $\psi = 0$, where n = 200 is sufficient). The very good agreement between the series

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(2.2) and the numerically integrated $10^{\circ} \times 10^{\circ}$ covariance function [formula (2.2)] is illustrated in Figure 2a-b. In Figure 2a we can distinguish between the two functions, in Figure 2b they coincide.

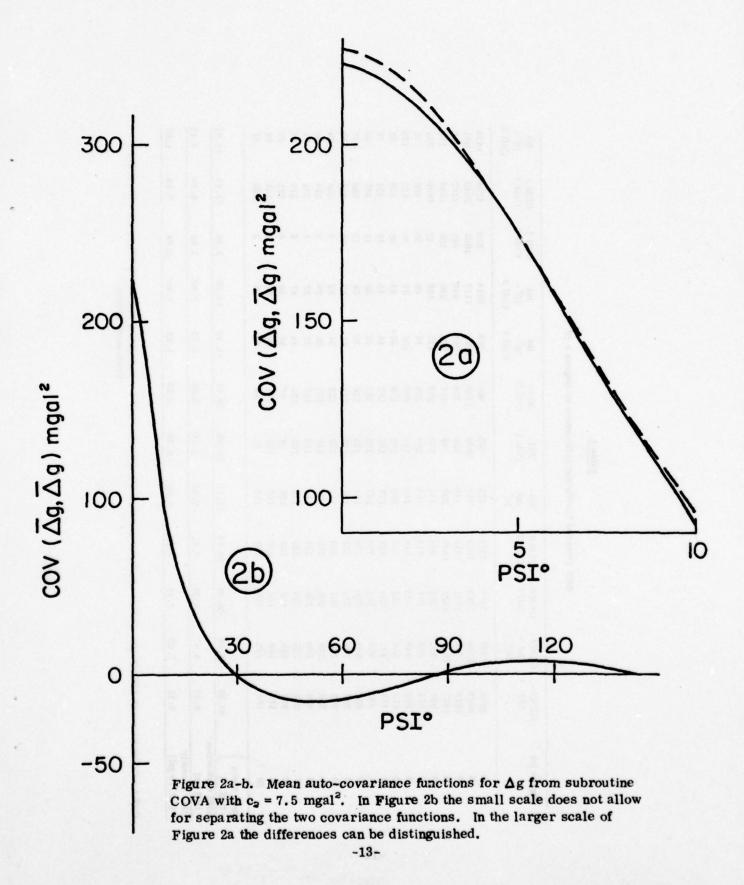
The spherical harmonic coefficients were determined to degree 20, both with mean elevations set to 0 (Table A. 1) and with the inclusion of approximate mean elevations (Table A. 2). (The approximate elevations were computed from the 5° anomaly data reported in Rapp (1977a).) We also computed the coefficients by collocation for zero elevation and no error covariance matrix included (Table A. 3). The tabulated coefficients refer to the sphere bounding the earth ellipsoid with a = 6378140 meters (cf. formula (3.2)). For comparison we determined also the coefficients from the 10° mean anomalies by the integration method described in Rapp (ibid.) [see also formulae (6.5 a-b)]. See Table A. 4.

In Table 1 we give the differences between different sets of potential coefficients. The relative mean differences give an over all view of the agreement between various sets of coefficients. It is obvious that the coefficients implied by the 5° anomalies (#251, Rapp, ibid.) agree slightly better with GEM 9 (Lerch et al., 1977) than those obtained from 10° anomalies. We also notice that the differences between the GEM 9 solutions and the solutions by collocation are less than the differences GEM 9 - Integrated 10° anomaly coefficients.

In Table 2 the potential coefficient solutions from 10° mean anomalies are compared relative to Kaula's rule. For low degree coefficients the differences between collocation (1 or 2) and integration is within 6% (except for n = 3). For higher degrees the discrepancies increase. In general, the inclusion of elevation information in collocation (Coll 1) seems to change the estimates a few percent. However, note the large discrepancies (10%) for n = 3. When the noise covariance matrix is excluded in collocation (Coll 3) the solution is clearly impared when compared with GEM 9. One could expect that the collocation 3 solution should agree better with the purely integrated coefficients than the other collocation solutions. We have no explanation of why this is not the case in the computations.

In Table 3 the RMS accuracy estimates by degree of the potential coefficients are compared. We notice that the accuracy estimates by collocation attenuate much slower than those implied by the integration method. Comparing the accuracy estimates of pure integration of 5° and 10° anomalies, we notice that the 10° estimates are smaller. As this result cannot agree with reality, it is likely to believe that the model used for computing the error estimates is too rough. The most obvious reason is probably that the covariances between the mean anomaly errors are disregarded. Although this is the case also in the collocation error estimates, the negative effect is less pronounced for these.

Finally, we compare the computation time for the determination of the potential coefficients from 10° mean anomalies (Table 4). The integration method is at least 30 times faster than collocation.



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Table 1

RMS Potential Coefficient Differences by Degree x 1010

	251	GEM 9-	GEM9-	GEM 9-	251- Int	251- Coll 1	251- Coll 2	Int 10°-	10°-	Coll 2	GEM 9-	10°
A I		10°			10°			Coll 1	Coll 2			Coll 3
2	2938	2897	3373	3514	522	603	801	206	1014	515	4268	1438
3	2625	2599	2646	1834	267	1056	1139	1101	11117	1085	2010	166
+	1612	1645	1741	1819	146	296	378	295	346	240	2162	746
2	1473	1549	1527	1549	802	340	317	223	240	109	1563	182
9	935	954	984	984	141	173	206	115	136	72	1006	241
7	574	694	101	111	194	204	206	84	65	55	720	73
80	592	546	523	516	145	194	200	100	97	35	529	123
6	612	526	525	522	200	179	179	64	54	20	538	63
10	444	427	425	432	173	181	187	44	45	18	424	16
11	332	377	381	378	147	129	127	47	20	15	383	20
12	254	249	256	259	124	124	126	32	29	13	258	47
13	222	232	223	221	124	120	121	41	42	10	234	32
14	252	249	251	253	112	122	123	34	32	80	259	38
15	228	270	266	265	138	137	137	53	59	7	278	56
16	202	236	220	221	118	116	1117	37	37	7	231	24
17	217	235	203	203	110	102	102	47	47	2	215	37
18	172	190	160	160	120	86	16	25	99	*	171	44
19	145	160	132	132	143	121	121	29	9	3	137	52
20	164	206	159	159	1115	85	84	02	70	3	166	61
Rel. Mean												
Diff. %	68.03	73.40	68.29	68.15	31.71	30.09	30.44	13, 43	13.59	3,49	71.17	14.91
RMS Undulation												
Diff [m]	8.72	8.81	9.20	8.81	2,03	2.76	3.00	2.35	2.62	2.05	9.88	3.15
RMS Anomaly Diff. [meal]	7.17	7.62	7.21	7.18	3 55	3 30	3.33	1.64	1.67	0.69	7.48	1.67

Coll 1 = Collocation with Elevations, Coll 2 = Collocation without Elevations, Coll 3 = Collocation without Elevations and without Noise Covariance Matrix

Table 2

Ratios between RMS Potential Coefficient Differences by Degree Implied by 10° Anomalies and $(C_{nm}, S_{nm}) = 10^{-5}/n^{2}$.

Units: Percent

Degree	Int-	Int-	Int-	Coll 1	l-	Degree	Int-	Int-	Int-	Coll 1-
	Coll 1	Coll 2	Coll 3							Coll 2
2	3	4	6	2		12	5	4	7	2
3	10	10	9	10		13	7	7	5	2
4	5	6	12	4		14	7	6	7	2
5	6	6	5	3		15	7	7	6	2
6	4	5	9	3		16	9	9	6	2
7	4	3	4	3		17	14	14	11	1
8	6	6	8	2		18	17	18	14	1
9	5	4	5	2		19	21	22	19	1
10	4	4	8	2		20	28	28	24	1
11	6	6	6	2						

Coll 1 = Collocation with Elevations

Coll 2 = Collocation without Elevations

Coll 3 = Collocation without Elevations or Noise Covariance Matrix

RMS Accuracy Estimates by Degree for Poter dial Coefficients

Degree	# 251	Int 10°	Coll 1	Coll 2
2	1911	1722	2054	1779
3	956	861	1674	2247
4	637	574	992	1207
5	478	430	691	807
6	382	344	468	438
7	318	286	443	486
8	273	245	370	378
9	239	214	341	360
10	212	190	301	300
11	191	171	285	289
12	173	155	272	277
13	159	142	266	266
14	147	130	250	248
15	136	121	243	243
16	127	113	237	237
17	119	105	231	231
18	112	100	224	224
19	106	94	217	217
20	100	89	209	209

Coll 1 = Collocation with Elevations Coll 2 = Collocation without Elevations All values multiplied by 10¹⁰

Table 4

Computation Times for Various Methods

Method	Degree of Expansion	CPU Time
Integration	25	19 ^s
Collocation with Elevations	20	12 ^M 13 ^s
Collocation without Elevations (COVA in Table)	20	9 [™] 21 ^s

Computer: IBM 370/168 No. of Observations: 416

6. An Extended View

An extension of the previous computations would be to determine the potential coefficients from 5° mean anomalies by collocation. However, as the number of observations then increases from 416 to 1654, it is no longer a standard procedure to invert the auto-covariance matrix of the system. Most computers cannot even store such a large matrix. We are going to estimate the necessary computer time as follows. In Table 5 the total number of necessary multiplications f(M) for computing the potential coefficients by collocation to degree n_0 for M observations are given. The direct method implies that the method of Cholesky is used for the inversion of the auto-covariance matrix. Let us assume that the total computer time T(M) is proportional to f(M). (We disregard the time needed for addition operations.) Then we obtain from Tables 4 and 5 for $n_0 = 20$ (no elevation information included):

$$T (1654) = \frac{T (416) f (1654)}{f (416)} = 3^h 50^m$$

Thus the necessary computer time is so large that we should really consider whether it could be reduced by modifying the method.

One possibility might be to determine the coefficients and their accuracy estimates according to:

(6.1)
$$\left\{\frac{\overline{C}_{na}}{\overline{S}_{nm}}\right\} = \left\{\frac{h_c^{\intercal}}{h_s^{\intercal}}\right\} \Delta \overline{g}$$

and

(6.2)
$$\left\{\frac{\overline{m}_{c}^{2}}{\overline{m}_{s}^{2}}\right\} = C_{0} - \left\{\frac{c_{c}^{\dagger} h_{c}}{c_{s}^{\dagger} h_{s}}\right\}$$

where the vectors of unknowns (hc and hs) are given by:

(6.3)
$${c_c \brace c_s} = (C + D) {h_c \brace h_s}$$

For each coefficient to be determined, the weights (h_c or h_s) can be computed iteratively by the following formula (cf. Miller, 1974):

(6.4)
$$h^{(\nu+1)} = h^{(\nu)} + \beta \{c - (C+D) h^{(\nu)}\}$$

where

 $0 < \beta < 2/\lambda_{max}$

 λ_{max} = maximum eigen value of C + D

 ν = iterative step: 0, 1, 2, ...

M = number of observations (mean anomalies)

The starting value $h^{(0)}$ for the iteration is most conveniently given in the spherical approximation. By assuming that all mean anomalies are located on the mean earth sphere of radius r_n we arrive at the following formula from (3.1b) after replacing Δg and \overline{C}_{nn} by $\Delta \overline{g}$ and $\beta_n \overline{C}_{nn}$, respectively [cf. Rapp, 1977a, formula (30)]:

(6.5a)
$$\overline{C}_{nm} = \sum_{k=1}^{M} h_{k}^{(0)} \Delta \overline{g}_{k}$$

where

(6.5b)
$$h_{k}^{(0)} = \frac{1}{4\pi\gamma\beta_{n}(r_{B}/r_{m})^{n+2}(n-1)} \iint_{\Delta\sigma_{k}} \overline{P}_{nm}(\sin\varphi) \cos m\lambda d\sigma$$

Substituting $\cos \underline{m} \lambda$ under the integral by $\sin \underline{m} \lambda$ we obtain the weights $(h_k^{(\circ)})$ for and coefficients \overline{S}_{nm} in (6.5b) and (6.5a), respectively. Even simpler approximations are obtained for:

(6.6)
$$h_{k}^{(0)} = \left(\frac{r_{m}}{r_{B}}\right)^{n+2} \overline{P}_{nm} \left(\sin \overline{\varphi}\right) \left\{\frac{\cos m \overline{\lambda}}{\sin m \overline{\lambda}}\right\} \Delta \sigma_{k} / [4\pi \gamma (n-1)]$$

which formula is given from (6.5b) by the approximation:

$$\frac{1}{\Delta\sigma_{k}} \iint_{\Delta\sigma_{k}} \overline{P}_{\text{nm}} \left(\sin \phi \right) \, \left\{ \begin{matrix} \cos m \lambda \\ \sin m \lambda \end{matrix} \right\} \, \, d\sigma \, \approx \, \, \boldsymbol{\beta}_{n} \, \, \overline{P}_{\text{nm}} \left(\sin \overline{\phi} \right) \, \left\{ \begin{matrix} \cos m \overline{\lambda} \\ \sin m \overline{\lambda} \end{matrix} \right\}$$

where $\overline{\varphi}$ and $\overline{\lambda}$ are given in (3.7). As the elevation of the highest mountain is less than 0.2% of the mean earth radius, we can expect that the iteration error in (6.4) is insignificant after a few iterations. Again, it should be emphasized that the spherical harmonic coefficients so determined refer to the Bjerhammar sphere (of radius r_B) and should be multiplied by $(r_B/a)^{n+2}$ in order to be consistant with other coefficient determinations, which usually refer to the sphere of radius a = 6378.140 km.

In the approximate formula (6.5b) and (6.6) we have disregarded the noise covariance function D. When considering the noise covariance function:

$$d(P,Q) = \sum_{n=2}^{\infty} d_n \beta_n^2 (r_B^2/r_P r_Q)^{n+2} P_n (\cos \psi_{PQ})$$

the following weight function can be derived for the spherical case [see the Appendix, formula (A.9)]:

(6.7)
$$h_{k}^{(o)} = \left(\frac{\mathbf{r}_{n}}{\mathbf{r}_{0}}\right)^{n+2} \frac{\mathbf{c}_{n}}{\mathbf{c}_{n} + \mathbf{d}_{n}} \overline{\mathbf{P}}_{nm} \left(\sin \varphi\right) \left\{\frac{\cos m \overline{\lambda}}{\sin m \overline{\lambda}}\right\} \Delta \sigma_{k} / 4\pi \gamma (n-1)$$

In the same way, if we assume that the errors between the blocks are uncorrelated, the following weight function can be derived [formula (A.11)]:

(6.8)
$$h_{k}^{(0)} = \frac{\Delta \sigma_{k}}{\gamma (n-1)4\pi} \left(\frac{r_{\theta}}{r_{m}}\right)^{n+2} \frac{c_{n} \beta_{n}^{2}}{c_{n} \beta_{n}^{2} \left(\frac{r_{\theta}}{r_{m}}\right)^{2(n+2)} + (2n+1)\epsilon_{k}^{2}} \overline{P}_{nm} (\sin \overline{\varphi}_{k}) \left\{\frac{\cos m \overline{\lambda}}{\sin m \overline{\lambda}}\right\}$$

where

 $\overline{\epsilon}_{k}^{2}$ = estimated mean square error of the observation in block k.

By using the iterative formula (6.4) we avoid the inversion of the auto-covariance matrix. Formula (6.5) is theoretically attractive in $h^{(0)}$, because it implies that the iterative collocation is carried out with the solution of the integration method as the original step.

Finally, we compare the number of necessary matrix ℓ erations for computing the coefficients and their accuracy estimates by direct collocation [formulae (3.4) and (4.3a-b)] and the proposed iterative method [formulae (6.1), (6.2) and (6.3)]. In the direct method the computations of the matrix inverse and the accuracy estimates are the most laborious operations. For the comparison we assume that $h^{(0)}$ of (6.4) is a priori given and that ν_0 steps are necessary in the iterative method. The numbers of necessary operations for a determination of the accuracy estimates to degree n_0 [i.e. for $(n_0+1)^2$ coefficients] are summarized in Table 5 (the direct method in accordance with Westlake, 1968, Table 7.1).

Table 5

Number of Necessary Matrix Operations to Compute Accuracy Estimates to Degree n_0

Operation	Direct Method (Cholesky)	Iterative Method [formulae (6.2) and (6.3)]
Addition	$M^3 - 2M^2 + M + (M^2 + M)(n_0 + 1)^2$	$\{(M+1) M\nu_0 + M\} (n_0 + 1)^2$
Multiplication	$\frac{1}{2}$ M ³ + $\frac{3}{2}$ M ² - M + 2M ² (n _o +1) ²	$(M^2 \nu_0 + M)(n_0 + 1)^2$

 ν_0 = number of iterative steps M = number of mean anomalies As the multiplications are the most time-consuming operations, we limit the following comparison to those figures. Then we obtain from the table that the iterative method is more efficient whenever:

$$(M \nu_0 + 1) M (n_0 + 1)^2 < \frac{1}{2} M^3 + \frac{3}{2} M^2 - M + 2 M^2 (n_0 + 1)^2$$

From this inequality we obtain

(6.8)
$$n_0 < \sqrt{\frac{M^2 + 3M - 2}{2M(\nu_0 - 2) + 2}} - 1$$

or, approximately, for $\nu_0 > 2$

(6.8')
$$n_0 < \sqrt{\frac{M+3}{2(\nu_0-2)}} - 1$$

Formula (6.8) is illustrated in Table 6.

Table 6

The Maximum Integer (n₀) Satisfying (6.8) for Various M and ν_0

$M \nu_0$	2	3	4	5	10
100	70	6	4	3	1
416	294	13	9	7	4
1000	707	21	14	11	6
1654	1169	27	19	15	9
5000	3535	49	34	27	16
10000	7071	69	49	39	24

no = maximum degree of series expansion

M = number of observations

 v_0 = number of iterative steps

The table shows that the iterative method is favorable merely for up to 2 or possibly 3 necessary iterations. However, as earlier discussed, the available approximations $h^{(0)}$ could very well meet such a requirement.

7. Conclusions

Geopotential coefficients determined by collocation were found to agree somewhat better with the GEM 9 coefficients than the coefficients determined by pure integration of 10° mean anomalies. This result is probably due to the incorporation of a weighting of the observations with respect to their a priori accuracies. However, this gain is achieved at the cost of several times more computation time.

By the inclusion of the elevation information in collocation, the coefficients to degree 20 changed by 3% on the average. A surprisingly large difference of 10% was obtained for n=3. The RMS changes of the undulation and the anomaly were 2 meters and 0.7 mgal, respectively. In general, however, we might expect that the 10° blocks give a too rough approximation to the topography to reveal any more significant magnitudes of the changes of the coefficients when including a correction for the topography (the Molodensky G_1 term). A possible explanation of the 10% differences for n=3 in various methods might be the non-symmetric distribution of the continents between the northern and the southern hemisphere.

From the comparison of the coefficient accuracy estimates for various methods (Table 3) we conclude that the error covariances between the mean anomalies should be taken into account in the computations by direct integration. In collocation it seems less important to include these covariances in the computations.

A natural continuation of the above study would be to compute the coefficients for 5° mean anomalies by collocation. However, due to the difficult task to invert an auto-covariance matrix for more than 1600 observations, the original method should first be modified according to the iterative method described in section 6. The method includes the solution by integration as a preliminary step. As this technique avoids the inversion of the auto-covariance matrix, a considerable gain in computer time can be expected. Another possibility would be to determine the auto-covariance matrix in an iterative way.

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Appendix

It is desired to determine the spherical harmonic coefficients (referring to the Bjerhammar sphere of radius r_B) implied by a mean anomaly field $\overline{\Delta g}$ on a sphere of radius r_B . The following covariance functions are given:

(A.1)
$$\left\{ \begin{array}{l} c_o \\ c_s \end{array} \right\} (P) = \left\{ \begin{array}{l} \cos \left(\overline{C}_{n'n'}, \overline{\Delta g_p} \right) \\ \cos \left(\overline{S}_{n'n'}, \overline{\Delta g_p} \right) \end{array} \right\} = b_{n'} \left(\begin{array}{l} r_g \\ r_p \end{array} \right)^{n+2} Y_{n'n'}(P)$$

where
$$b_{n'} = c_{n'} \beta_{n'} / \gamma (2n'+1) (n'-1)$$

$$Y_{n'n'}(P) = P_{n'|n'|}(\sin \phi_P) \begin{cases} \cos m' \lambda P \\ \sin |m'| \lambda P \end{cases}$$

(A.2)
$$c(Q, P) = cov(\overline{\Delta g_Q}, \overline{\Delta g_P}) = \sum_{n=2}^{\infty} c_n \beta_n^2 (r_B^2/r_Q r_P)^{n+2} P_n(\cos \varphi_{QP})$$

and

(A.3)
$$d(Q, P) = cov (\epsilon_Q, \epsilon_P) = \sum_{n=2}^{\infty} d_n \beta_n^2 (r_B^2/r_Q r_P)^{n+2} P_n (cos \varphi_{QP})$$

The solutions for $\overline{C}_{n'n'}$ and $\overline{S}_{n'n'}$ by the method of least squares collocation are given by (see Sjöberg, 1978)

$$\left\{ \begin{matrix} A.4 \\ A.4 \end{matrix} \right\} = \frac{1}{4\pi} \int \int \left\{ \begin{matrix} h_c (Q) \\ h_s (Q) \end{matrix} \right\} \overline{\Delta g} (Q) d\sigma_Q$$

where the weight functions h_c (Q) and h_s (Q) are given by h(Q) of the following Wiener-Hopf integral equations

(A.5)
$$\left\{ \begin{array}{l} c_c \\ c_s \end{array} \right\} (P) = \frac{1}{4\pi} \int \int h(Q) \left\{ c(Q, P) + d(Q, P) \right\} d\sigma_Q$$

<u>Proposition 1:</u> The weight functions for C_{nm} and S_{nm} in (A.4) implied by (A.1) - (A.3) and (A.5) for $r_p = r_q = r_m = constant$ are given by:

(A.6)
$$h(Q) = \left(\frac{r_n}{r_n}\right)^{n+2} \frac{c_n}{c_n + d_n} Y_{nn}(Q) / \gamma \beta_n(n-1)$$

Proof: We expand (A.2) and (A.3) accordingly:

(A.2')
$$c(Q, P) = \sum_{n=2}^{\infty} \sum_{n=-n}^{n} \frac{c_n R_n^2}{2n+1} \left(\frac{r_0}{r_n}\right)^{2(n+2)} Y_{nn}(Q) Y_{nn}(P)$$

and

(A.3')
$$d(Q, P) = \sum_{n=2}^{\infty} \sum_{n=-n}^{n} \frac{d_{n} \beta_{n}^{2}}{2n+1} \left(\frac{r_{\theta}}{r_{n}}\right)^{3(n+2)} Y_{nn}(Q) Y_{nn}(P)$$

(A.7)
$$\frac{1}{4\pi} \iint Y_{n,n} Y_{p,q} d\sigma = \begin{cases} 1 & \text{if } n = p \text{ and } m = q \\ 0 & \text{otherwise} \end{cases}$$

Inserting (A.1), (A.2'), (A.3') and the expansion

$$h(Q) = \sum_{n=0}^{\infty} \sum_{n=-n}^{n} h_{n} Y_{n}(Q)$$

into (A.5) we obtain from (A.7):

(A.8)
$$b_{n'}(r_B/r_m)^{n+2} Y_{n'n'}(P) = \sum_{n,m} b_{nn} \frac{c_n + d_n}{(2n+1)} \beta_n^2 (r_B/r_m)^{2(n+2)} Y_{nn}(P)$$

This identity is satisfied by

$$h_{n} = \begin{cases} \frac{c_n}{c_n + d_n} \left(\frac{r_n}{r_n}\right)^{n+2} / \gamma \beta_n \quad (n-1) & \text{if } n = n' \text{ and } m = m' \\ 0 & \text{otherwise} \end{cases}$$

The proposition follows from this result.

Using the following approximation (cf. Meissl, 1971, pp. 22-23)

$$\frac{1}{\Delta\sigma} \iint_{\Delta\sigma} Y_{n \cdot n}(Q) d\sigma_{Q} = \beta_{n} Y_{n \cdot n}(\overline{Q})$$

where \overline{Q} is the center of the block $\Delta\sigma$, we obtain the following relation from (A. 6):

(A.9)
$$\frac{1}{4\pi} \iint_{\Delta \sigma_{k}} h(Q) d\sigma = \left(\frac{\mathbf{r}_{n}}{\mathbf{r}_{B}}\right)^{n+2} \frac{\mathbf{c}_{n}}{\mathbf{c}_{n} + \mathbf{d}_{n}} Y_{nn}(\overline{Q}_{k}) \Delta \sigma_{k} / 4\pi \gamma (n-1)$$

$$-26-$$

Corollary 1: For d(Q, P) of Proposition 1 replaced by

$$d(Q, P) = \epsilon^2(Q) \delta(\psi_{QP})$$

where $\delta(\psi_{QP})$ is the Dirac delta function, we obtain

(A.10)
$$h(Q) = \frac{c_n \beta_n}{\gamma(n-1)} \left(\frac{r_B}{r_m}\right)^{n+2} \frac{1}{c_n \beta_n^2 (r_B/r_m)^{2(n+2)} + (2n+1) \epsilon^2(Q)} Y_{n_m}(Q)$$

Proof: As

$$\frac{1}{4\pi} \int \int \epsilon^{2} (Q) \delta(\psi_{QP}) Y_{nm}(Q) d\sigma_{Q} = \epsilon^{2} (P) Y_{nm}(P)$$

formula (A. 8) becomes in this case

$$b_{n}'(\mathbf{r}_{B}/\mathbf{r}_{m})^{n'+2} Y_{n'm'}(P) \equiv \sum_{n\neq m} h_{nm} \left(\frac{c_{n}}{2n+1} \beta_{n}^{2} \left(\frac{\mathbf{r}_{B}}{\mathbf{r}_{m}}\right)^{2(n+2)} + \epsilon^{2}(P)\right) Y_{nm}(P)$$

and the proof follows after noting that

$$h_{nm} = 0$$
 for $n \neq n'$ and $m \neq m'$.

In accordance with formula (A.9) we obtain in this case:

$$(A.11) \qquad \frac{1}{4\pi} \iint h(Q) d\sigma \approx \frac{c_n \beta_n^2}{\gamma(n-1)} \left(\frac{r_{\text{B}}}{r_{\text{m}}}\right)^{n+2} \frac{1}{c_n \beta_n^2 (r_{\text{B}}/r_{\text{m}})^2 (n+2) + (2n+1) \epsilon^2 (\overline{Q}_k)} Y_{n\text{m}} (\overline{Q}_k) \frac{\Delta \sigma_k}{4\pi}$$

<u>Proposition 2:</u> The error estimates for \hat{C}_{nu} and \hat{S}_{nu} of (A.4) and (A.5) are given by

$$\overline{m}^2 = C_0 - \frac{1}{16\pi^2} \iiint h(Q) \ h(Q') \left\{ c(Q,Q') + d(Q,Q') \right\} \ d\sigma_Q \ d\sigma_Q.$$

where Co is the a priori variance of the coefficients.

Proof: We consider only the estimate \hat{C}_{nn} .

$$\overline{\mathbf{m}}_{\mathbf{c}}^{2} = \mathbf{E} \left\{ \left(\overset{\wedge}{\mathbf{C}}_{\mathbf{nm}} - \overline{\mathbf{C}}_{\mathbf{nm}} \right)^{2} \right\} = \mathbf{E} \left\{ \overline{\mathbf{C}}_{\mathbf{nm}}^{2} \right\} + \mathbf{E} \left\{ \overset{\wedge}{\mathbf{C}}_{\mathbf{nm}}^{2} \right\} - 2 \mathbf{E} \left\{ \overline{\mathbf{C}}_{\mathbf{nm}} \overset{\wedge}{\mathbf{C}}_{\mathbf{nm}} \right\}$$

where
$$\begin{split} E\left\{\overline{C}_{nn}^{\ 2}\right\} &= C_0 \\ E\left\{\overline{C}_{nn}^{\ 2}\right\} &= \frac{1}{16\pi^2} \iiint h(Q) \ h(Q) \ E\left\{\overline{\Delta g}_Q \ \overline{\Delta g}_Q \right\} d\sigma_Q \ d\sigma_Q \ , \\ &= \frac{1}{16\pi^2} \iiint h(Q) \ h(Q) \ \left\{c(Q,Q) + d(Q,Q)\right\} d\sigma_Q \ d\sigma_Q \ , \end{split}$$
 and
$$\begin{split} E\left\{\overline{C}_{nn}^{\ 2}\right\} &= \frac{1}{4\pi} \iiint h(Q) \ E\left\{\overline{C}_{nn} \ \overline{\Delta g}_Q\right\} d\sigma_Q \\ &= \frac{1}{4\pi} \iint h(Q) \ c_c(Q) \ d\sigma_Q \\ &= \frac{1}{16\pi^2} \iiint h(Q) \ h(Q) \ \left\{c(Q,Q) + d(Q,Q)\right\} d\sigma_Q \ d\sigma_Q \ , \end{split}$$

From these deductions the proposition follows immediately.

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Table A.1: Fully Normalized Geopotential Coefficients Determined from 416 10° Mean Anomalies by Collocation. No Mean Elevations Included. All Coefficients multiplied by 10° . a=6378140 m.

M	n	C	9	SICTA	SICHA	N	M	c	6	BICMA	SICMA
2		-483.4460		0.2016 .							
22353	1	0.3000	-0.0906	9.1799	0.1788	2	2	2.4488	-1.3057	0.1678	0.1897
3		9.7133		0.2304		-	-			0.1010	0.1077
3	1	1.8349	0.1254	0.2263	0.2261	3	2	1.1793	-0.4719	0.2263	0.2243
	3		1.5310	0.2193	0.2203						
*	1	0.8957 -0.4564	-0.4057	0.1324			-				
445555	3	0.7955	-0.3966	0.1219	0.1217	:	2	0.3170 -0.2265	0.3939	9. 1225	0.1227
5	•	0.2236	-0.0700	0.0096	0.1100		•	-0.2200	0.4.00	0.1151	0.1141
5	1	-0.1576	-0.2482	0.9821	0.0817	5	2	0.4107	-0.2016	0.0020	0.0824
5	3	-0.2448	-0.1369	0.0011	0.0811	5	4	-0.0921	-0.0276	9.0771	0.0769
	5	0.1064	-0.4974	0.0740	0.0766						
6		-0.1376		0.0540							
6	3	0.1128	0.9635	9.0466	0.0457	6	2	0.2816	-0.3645	0.0464	0.0459
2	5	-0.0173 -0.3760	-0.0625 -0.5370	0.0459	0.0435	6	6	-0.1800 0.0097	-0.4041	0.0426	0.0423
7		0.2002	-0.0010	0.0547	0.0370	•		0.0071	-0.2402	4.0371	0.0375
7	1	0.2018	0.0466	0.0513	0.0510	7	2	0.2858	0.1194	0.0497	0.0499
7	3	0.1615	-0.1805	0.0501	0.0301	7	4	-0.1572	-0.1660	0.0490	0.04(19
7	5	0.0896	-0.0060	0.0466	0.0472	7	6	-0.3078	0.2000	0.0448	0.0449
7777088	7	-0.0325	-0.0921	0.0450	0.0449						
8		0.0422		0.0441			_				
8	3	-0.0423	0.9575	0.0492	0.0400	0	2	0.1353	0.0995	0.0399	0.8404
	5	-0.9176	0.0345	0.038A 0.0366	0.0385	8	6	-0.2167	0.0515	0.0392	0.0307
899999	7	0.0383	0.0713	9.0338	0.0375	8	å	-0.0006 -0.1417	0.1988	9.0358 9.0345	0.0354
4	•	0.1336	0.0	0.0409	0.0000	.0		-4.1411	0.0711	W. 0343	0.0338
9	1	0.1723	-0.0228	0.0382	0.0301	9	2	0.1171	-0.0843	0.0300	0.0384
9	3	-0.1786	-0.0305	0.0373	0.0372		4	-0.0398	0.0490	9.0368	0.0363
9	2	-0.0572	-0.0336	0.0362	0.0367	9	6	0.0014	0.1823	0.0347	0.0344
9	7	-0.0023	-0.0215	9.0336	0.0336	9	U	0.2038	0.0065	0.0327	0.0324
	9	-0.0159	0.0237	0.0333	0.0333						
10	1	9.0303	-0.0147	0.0331			-				
10	3	-0.9416	-0.0954	0.0326	0.0328	10	2	-0.0657 -0.0674	-0.0457	0.0324	0.0326 0.0303
10	5	-0.0261	-0.0113	0.0301	0.0306	10	6	-0.0475	-0.0479	0.0299	0.0296
10	7	9.0024	-0.0187	0.0278	0.0279	10	8	0.0413	-0.0533	0.0275	0.0270
10	9	0.1013	-0.0222	0.0263	0.0265	10	10	0.1159	-0.0309	0.9277	0.0274
11		-0.0933		0.0336							
11	1	-0.0214	0.0197	0.0310	0.0311	11	2	-9.0219	-0.0922	0.0317	0.0310
!!	3	-0.0747	-0.1126	0.0306	0.0304	!!	•	-0.1044	-0.0787	0.0302	0.0299
11	8	0.0123	-0.105B	0.0288	0.0292	11	6	0.0092	0.0100	0.0289	0.0207
ii	•	-0.0456	Ø. 0B17	0.0263	9.0264	11	10	-9.0269	9.0613	9.0266 9.0263	0.0253
ii	11	0.0769	-0.0164	0.0271	0.0271				4.4.00	0.0200	V. V23.
12		0.0330		0.0321							
12	1	-0.0213	-0.0334	9.0247	0.0298	12	2	●. 9038	-0.0309	0.0303	0.0306
12	3	0.0097	0.0387	0.0295	0.0294	12	4	-0.0653	-0.0343	0.0288	0.0207
12	2	0.0376	-0.0023	0.0281	0.0203	12		0.0253	0.0496	0.0275	9.0272
12	7	-0.0240	0.0267	0.0272	0.0271	12	.8	0.0100	0.0264	0.0263	0.0261
12	11	0.0106	0.0169	0.0252	9.0251	12	10	-0.0094	-0.0265	9.0254	0.0203
15		0.0473	0.0007	0.0303	0.0231	12	12	0.0134	-9.0094	0.0265	0.0264
13	1	-0.0016	0.0186	0.02110	0.0292	13	2	9.0085	-0.0414	0.0289	0.0293
iā	å	-0.0144	0.0421	0.0287	9.0206	13	-	0.0019	-0.0060	0.0277	0.0275
13	8	0.0386	0.0397	0.0271	0.0273	13	6	-0.0246	-0.0086	0.0265	0.0265
13	7	-0.0171	0.0157	0.0239	0.0239	13	Ö	-0.0237	0.0200	0.0258	0.0255
13	9	-0.0140	0.0354	9.0248	9.0247	13	10	0.0359	-0.0149	0.0243	0.0240
13	11	0.0043	0.0201	0.0245	0.0246	13	12	-9.0016	0.8943	0.0242	0.0245
	13	-0.0347	0.0637	0.0257	0.0260						
14		0.0000		9.02110							

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14 1	0.0204	0.0084	0.0276	9.9289	14 2	-0.0307	-0.0173	0.0272	0.0272
14 3	0.0096	0.0082	9.0272	0.0270	14 2	-0.0016	-0.0280	9.0263	0.0260
14 5	0.0147	-0.0070	0.0254	0.0254	14 6	-0.00B5	0.0010	0.0251	0.0250
14 7	0.0342	-0.0140	0.0242	0.0241	14 0		-0.0234	0.0240	0. 6237
14 9	0.0154	0.0416	0.0234	0.0234	14 10		-0.0036	0.0228	9.0225
14 11	9.0336 9.0365	0.0287	0.0224	0.0223	14 14		-0.0205	9.0244	0.0231
13	-0.0027	0.0207	0.0259	0.0220	14 14	-0.0171	0.0117	9.0244	0.0245
15 1	0.0337	0.0269	0.0270	0.0274	15 2	0.0045	0.0133	0.0266	0.0267
1: 3	0.0441	0.0452	0.0262	0.0262	15 4		-0 0129	9. 9269	0.0258
13 6	0.0997	0.0133	0.0247	0.0248	15 6		0254	8.0245	0.0246
15 7	0.0563	0.0118	0.0240	0.0239	15 0		J.0198	0.0234	0.0231
15 9	9.0024 -0.0043	0.9114	0.0230	6.0231 6.0220	15 10 15 12		0.0646	0.0226	6.0220
15 13	-0.9183	0.0177	0.9220	W. 0226	10 14		-0.0212	0.9227	0.0227
15 15	-0.0263	0.0083	0.0244	0.0243					
16	0.0214		0.0234						
16 1	-0.0083	0.0170	0.0268	0.0270	16 2		0.0019	0.0258	0.0258
16 3	-0.0176 -0.0123	0.0246	9.0256	9.0256	16 4	0.0314	0.0619	0.9252	0.0252
16 5	-0.0118	-0.0064	0.0245	0.0245	16 6 16 8		0.0349	0.0237	0.0239 0.0223
16 9	-0.0049	-0.0589	0.0222	0.0226	16 19		-0.0083	9.0224	0.0223
16 11	0.0064	-0.0104	0.0221	0.0217	16 12		0.0912	0.0217	0.0216
16 13	0.0011	0.0153	0.0221	9.0213	16 14	-9.9018	-0.0239	9.0225	0.0224
16 15	-0.0098	-0.0335	0.0231	0.0219	16 16	-0.0178	-0.0172	0.0242	0.0249
17	0.0019		0.0197						
17 1	0.0054	0.0228	0.0296	0.0277	17 4	-0.0307 -0.0194	0.0298	0.0217	9.0230
17 5	-0.0163	0.0114	0.0247	0.0248	17 6		-0.0351	0.0220	0.0230
17 7	0.0192	-0.0231	0.0231	0.0232	17 0		-0.0092	0.0226	0.0224
17 9	-0.01111	-0.0336	0.0218	0.0222	17 19	-0.0110	0.0128	0.0218	0.0217
17 11	-0.0013	0.0034	0.0219	0.0214	17 12	-0.0166	0.0002	0.0213	0.0212
17 13	0.0174	0.0102	0.0222	0.0204	17 14		0.0198	0.9215	0.0215
17 13	0.0146	0.0172	0.0235	0.0200	17 16	-0.0112	0.0141	0.0223	0.0222
18	0.0069	0.0001	0.0302	0.72.77					
18 1	-0.0199	-0.0390	0.0165	0.0167	18 2	-0.0054	0.0039	0.0309	0.0309
10 3	-0.0030	-0.0107	0.0153	0.0154	10 2	9.0064	0.0053	0.0292	0.0292
18 5	0.0044	0.0138	0.01112	0.0103	18 6		-0.0022	0.0256	0.0256
18 7	-0.0016 0.0058	-0.0010	0.0206	0.0206	10 0		-0.0076	0.0229	0.0220
10 11	-0.0211	0.0087 -0.0076	0.0210	0.0213	18 10 18 12	0.0184	-0.0049	0.0214	0.0213
18 13	-0.0032	-0.0520	9.0225	0.0100	18 14	0.0022	-0.0193	0.0209	0.0210
18 13	-0.0419	-0.0271	0.0237	0.0102	10 16		0.0129	0.0219	0.0217
18 17	0.0091	-0.0097	0.0220	0.0217	18 18	-0.0041	-0.0116	0.0292	0.0151
19	0.0001		0.0253						
19 1	0.0007	-0.0176	0.0216	0.0217 0.0237	19 2		-0.0094	9.0247	0.0247
.17 5	-0.0089	0.0049	0.0269	0.0267	19 4		0.0166	0.0197	0.0197
19 7	-0.0026	0.0045	9.0259	0.0259	19 B		0.0013	0.0179	9.0179
19 9	0.0049	0.0039	0.0220	0.0231	19 10		-0.0092	0.0198	0.0198
19 11	0.0003	0.0060	0.0210	0.0200	19 12		-0.0030	0.0204	0.0202
19 13	0.0077	-0.0203	0.0230	0.0173	19 14		-0.0066	0.0202	0.0203
19 13	0.0007	-0.0155	0.0241	0.0163	19 16		0.0009	0.0208	0.0206
19 17	0.0100	0.0095	0.0214	0.0213	19 10	0.0336	-0.0092	0.02.0	0.0197
20	-0.0036	0.0070	0.0234	17,11220					
20 1	-0.0119	-0.0031	0.0216	0.0216	20 2	-0.0036	0.0033	0.0227	0.0227
29 3	-0.0076	0.0007	0.0233	0.0233	20 4	-0.0050	-0.0193	0.0198	0.0198
20 6	-0.0040	0.0011	0.0230	0.0230	20 6		0.0036	0.0221	0.0221
20 7	-0.0179	-0.0065	0.0178	9.0179	20 8		0.0142	0.0244	0.0245
29 11	0.0202	0.0037	0.0161	0.0163	20 12		0.0078	0.0226	0.0204
20 13	0.0039	-0.0004	0.0223	0.0162	20 14		-0.0019	0.0198	0.0199
20 15	0.0005	-0.0074	0.0228	0.0159	20 16	-0.0163	-0.0090	0.0200	0.0201
20 17	-0.0014	0.0067	0.0202	0.0202	20 18	-0.0094	-0.0189	0.0218	0.0196
20 19	-0.0033	0.0911	0.0208	0.0208	20 20	0.8152	0.0043	0.0217	0.0218

Table A.2: Fully Normalized Geopotential Coefficients Determined from 416 10° Mean Anomalies by Collocation. Approximate Mean Elevations Included. All coefficients multiplied by 10° . a = 6378140 m.

M	M	C	8	BICMA	BICMA	N	M	C	8	BICMA	BICHA
2		-483.4651		0.2212							
1110000+++0000	1	0.2721	-0.0049	0.2098	0.2196	2	2	2,3810	-1.3976	9. 1927	9.1806
3		0.6295		6.1772							
3	1	1.0080	-0.6201	9.1730	0.1604	3	2	1.3741	-0.54/2	0.1674	0.1690
3	3	0.6623	1.5512	0.1580	0.1662						
•		0.8659		0.1096							
•	1	-0.4433	-0.3807	0.1001	0. 9967	:	2	0.3700	0.4065	0.1036	0.1019
:	3	0.7904	-0.3962	0.0947	0.0976	•	4	-0.2159	0.3966	0.0968	0.0903
3	1	0.2038	-0.2469	0.0699	0.0673	5	2	0.4138	-0.1989	0.0721	0.0705
-	3	-0.2435	-0.1402	0.0694	0.0709	5	4	-0.0911	-0.0495	0.0662	0.0645
×	5	0.1198	-0.4990	0.0617	9.0667	•	•	-0.0711	-0.0473	0.0002	0.0050
		-0.1464	0.4	0.0583	0.000.						
6666	1	0.1175	0.0490	0.0480	9.0486	6	2	0.2776	-0.3591	0.0490	0.0489
6	3	-0.0168	-0.0632	0.0487	0.0485	6	4	-0.1730	-0.4046	0.0455	0.0459
6	5	-0.3857	-0.5336	0.0399	0.0424	6	6	0.0041	-0.2293	0.0402	0.0407
7		0.2042		0.0504							
7		0.2090	0.0453	0.0473	0.0460	7	2	0.2941	0.1235	0.0450	0.0450
7	3	0.1597	-0.1926	0.6452	9.0455	7	4	-0.1582	-0.1714	0.0450	0.0448
7	3	0.0835	-0.0001	0.0421	0.0434	7	6	-0.3094	0.2030	0.0410	0.0401
777770	7	-0.0367	-0.0903	0.0411	0.0414						
	1	-0.0410	0.0544	0.0438	0.0391	8	2	0.1375	9.1005	0.0389	0.0392
	3	0.0795	-0.0228	0.0378	e. 0375	8	4	-0.2114	0.0454	0.0384	9.0378
ä	5	-0.0193	0.0311	0.0339	0.0369	ä	6	-0.0063	0.2006	0.0347	0.0345
888	7	0.0445	9.0735	0.0336	6.0328	a	8	-0.1438	0.0959	0.0344	0.0331
		0.1377	0.0100	0.0391	0.0020	••		0.1400	0.0,0,	0.0044	0.0351
9		0. 1770	-0.0223	0.0364	0.0360	9	2	0.1169	-6.0136	0.0369	0.0365
4	3	-0.1794	-0.0320	0.0351	0.0350	9	4	-0.0619	0.0510	0.0348	0.0342
"	5	-0.0394	-0.0361	0.0343	0.0349	9	6	0.0807	0.1823	0.0330	0.0325
4	7	-0.0827	-0.0223	0.0318	0.0317	9	13	0.2041	0.0072	0.0310	0.0304
9	9	-0.0179	0.0253	0.6314	0.0317						
10		0.0264		0.0353			_				
10	1	0.1151	-0.6175	6.0328	0.0328	10	2	-0.0667	-0.0425	0.0323	0.0326
10	3	-0.0419	-0.0978	0.0319	0.0319	10	6	-0.0704	-0.0950	0.0309	0.0305
10	5	-0.0270 0.6828	-0.0118	0.0302	0.0307	10	å	-0.0492 0.0410	-0.0524	0.0299	0.0297
10	6	0.1031	-0.0220	0.0265	0.0267	10	10	0.1172	-0.0335	0.027B	0.0272
ii		-0.0966	-0.0220	0.0332	₩.₩201		10	0.1112	-0.0333	0.0210	0.0273
ii	1	-0.0221	0.0074	0.0307	0.0307	11	2	-0.0208	-0.0925	0.0312	0.0314
ii	3	-0.0741	-0.1140	0.0302	0.0300	ii	4	-0.1059	-0.0798	0.0297	0.0294
ii	5	0.0114	0.0070	0.0284	0.0280	11	6	-0.0107	0.0098	0.6285	0.0283
11	7	0.0372	-0.1035	0.0276	0.0276	11	n	0.0099	0.0609	0.0263	0.0250
11	9	-0.0494	0.0821	0.0259	0.0261	11	10	-0.0250	0.0136	0.0260	0.0250
11	11	0.0766	-0.0169	0.0267	6.0269						
1222222		0.0312		0.0317			1				
12	1	-0.0245	-0.0337	0.0294	0.0293	12	2	0.0053	-0.0303	0.0298	0.0302
12	3	0.0114	0.0388	0.0290	0.6289	12	•	-0.0650	-0.0350	0.0283	0.0282
12	5	0.0365	-0.0022	0.0275	0.027B	12	6	0.0272	0.0490	0.0270	0.0267
12	7	-0.0249	0.0277	0.0267	0.0267	12	10	-0.0092	-0.0269	0.0259	0.0256
13	ıĭ	0.0108	0.0060	0.0246	0.0247	12	12	9.0140	-0.0106	0.0250	0.0248
12		0.0469	0.0000	0.0299	0.0277	10		0.0140	0.0100	0.0201	0.0269
13	1	-0.0020	0.0183	0.0204	0.0287	13	2	0.0095	-0.0421	0.0284	0.0289
13	3	-0.0135	0.0413	0.0203	0.0202	13	-	0.0024	-0.0069	0.0273	0.0270
13	5	0.0593	0.0406	0.0266	0.0269	13	6	-0.0245	-0.0092	0.0261	0.0259
13	7	-0.0172	0.0163	0.0255	0.0254	13	8	-0.0254	0.0199	9.0254	0.0250
13	9	-0.0137	0.0347	0.0244	0.0243	13	10	0.0351	-0.0129	0.6239	0.0235
13	11	0.0047	0:0204	0.0241	0.0242	13	12	-0.0004	0.0966	0.6238	0.0241
13	13	-0.0345	0.0650	0.0255	0.0256						
14		-0.0007		0.0201							

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14	1	0.0192	0.0074	0.0277	0.0280	14	2	-0.0379	-0.0164	0.0273	0.0274
14	3	0.0103	0.0095	0.0272	0.0271	14	4	-0.0014	-0.0273	0.6263	6.0261
14	5	0.0157	-0.0069	0.0255	0.0255	14	6	-0.0092	0.0013	6.0251	0.0251
14	7	6.0334	-0.0145	0.0243	0.0242	14	8	-0.0275	-0.0243	0.0241	0.0236
14	4	0,0157	0.0411	0.0236	0.0235		10	0.0157	-0.0040	0.0230	0.0226
14	11	0.0327	-0.0742	0.0225	0.0225		12	0.0005	-6.0204	0.0229	0.0232
14	13	0.0370	0.0306	0.0230	0.0230	14	14	-0.0104	0.0123	0.0245	0.6247
15		-0.0036		0.0269							
13	1	0.0340	0.0267	0.0270	0.0273	15	2	0.0047	0.0137	0.020+	0.0268
13	3	0,0446	0.0449	0.0262	0.0263	15	4	0.0031	-0.0120	0.0259	0.0250
13	5	0.0104	0.0135	0.0247	0.0248	15	6	-0.0075	0.0253	6.0245	0.0246
13	7	0.0359	0.0124	0.6239	0.0239	15	8	-0.9439	0.0194	0.0234	0.6231
15	9	0.0027	-0.0029	0.0230	0.0232	15	10	-0.0151	-0.0006	0.0226	0.0226
15	11	-0.0064	0.0107	0.0223	0.0220	15	12	-0. 107	9.0649	0.0221	0.0221
15	13	-0.0179	0.0179	0.0229	0.0226		14	0.0119	-0.0200	0.0227	0.0227
15	15	-0.0262	0.0071	0.0245	0.0243		-				
16		0.0203		0.0254							
10		-0.0089	0.0137	0.0260	0.0279	16	2	-0.0105	0.0035	0.0258	0.0258
16	3	-0.0174	0.0233	0.0256	0.0256	16	4	0.0317	0.0619	0.0252	0.0231
16	5	-0.0111	0.0204	0.0245	0.0245	16	6	-0.0026	-0.0322	0.6237	0.0239
16	7	-0.0125	-0.0055	0.0235	0.0236	16	8	-0.0505	0.0338	0.0229	0.0228
16	٠	-0.0032	-0.0586	0.0223	0.0226		10	-0.0062	-0.0093	6.0224	6.6223
16	11	0.0060	-0.0113	0.0221	0.0217		12	0.0156	0.0005	0.0218	0.0216
16	ià	0.0010	0.0153	0.0221	0.0215		14	-0.0019	-9.0238	0.0225	
16	15	-0.0107		0.0231	0.0219						8.6225
	12	0.0020	-0.0338		0.0219	16	16	-0.0173	-0.0172	0.0242	0.0240
17				0.0197			-				
17	1	0.0053	0.0226	0.0295	0.0296	17	2	-0.0385	0.0176	0.0217	0.0217
17	3	0.0048	-0.0144			17	4	-0.0186	0.0308	0.0231	0.9230
17		-0.0161	0.0111	0.0247	0.0248	17	6	-0.0213	-0.0357	0.0228	0.0229
17	7	0.0188	-6.0234	0.0231	0.0231	17	8	0.0211	-0.0095	0.0225	0.0224
17	9	-0.0175	-0.0355	0.0217	0.0222		10	-0.0110	0.0127	0.0217	0.0217
17	11	-0.0011	0.0035	0.0219	0.0214		12	-0.0167	0.0002	0.0213	0.0212
17	13	0.0100	0.0105	0.0222	0.0204		14	-0.0126	0.0183	0.0215	0.0215
17	15	0.0145	0.0166	0.0235	0.0208	17	16	-0.0112	0.0134	0.0222	0.0222
17	17	-0.0314	0.0060	0.0238	0.0237						
111		0.0066		0.0302		Due-					
111	1	-0.0200	-0.0390	0.0165	0.0166	14)	2	-0.0054	0.0042	0.0309	0.0309
141	3	-0.0068	-0.0106	0.0153	0.0153	18	4	0.0060	0.0037	0.0292	6.0292
111	5	0.0043	0.0142	0.0181	0.0182	10	6	0.0165	-0.0027	0.0256	0.0256
111	7	-0.0015	-0.0023	0.0203	0.0206	18	B	0.0281	-0.0077	0.0229	0.0228
188	9	0.0065	0.0094	0.0210	0.0214		10	0.0184	-0.0042	0.0214	0.0213
113	11	-0.0210	-0.0076	0.0212	0.0203		12	0.0056	-0.0172	0.0211	0.0209
.18	13	-0.0055	-0.0525	0.0225	0.0188		14	0.0022	-0.0194	0.0209	0.0210
111	13	-0.0413	-0.0281	6.0237	0.0182		16	0.0103	0.0126	0.0219	0.0217
113	17	0.0093	-0.0093	0.0220	9.0217	18	18	-0.0044	-0.0124	0.0292	0.0150
1.3		-0.0003	the beautiful	0.6263							
19	1	0.0001	0.0174	0.0216	0.0217	19	3	0.0209	-0.0098	0.0247	0.0247
19	3	0.0001	-0.0138	0.0237	0.0237	19	4	0.0163	-0.0116	6.0197	8.0196
19		-0.0000	0.0049	0.0269	0.0269	19	6	0.0060	9.0166	0.0159	0.0160
19	7	-0.0025	0.0042	0.0239	0.0239	19	8	0.0222	0.0017	0.0179	0.0178
19	9	0.0049	6.0043	0.0227	6,0230	19	10	-0.0134	-0.0091	0.0198	0.0197
19	11	0.0007	0.0058	0.0210	0.0200	19	12	-0.0018	-2.0031	0.0204	0.0202
19	13	0.0082	-0.0294	0.0230	0.0174		14	0.0161	-0.0065	0.0201	0.0202
19	15	0.0010	-0.0160	0.0241	0.0163		16	-0.0243	B. 0091	0.0208	0.0206
19	17	0.0194	-0.0063	0.0214	0.0212		18	0.0336	-0.0092	0.0230	0.0196
19	19	0.0199	0.0091	0.0226	0.0226				0.00.0	0.0200	0.0170
20	-	-0.0056		0.0234							
20	1	-0.0129	-0.0036	0.0216	0.0216	20	2	-0.0036	0.0029	0.0227	0.0227
2.1	3	-0.0070	0.0001	0.0233	0.0233	20	4	-0.0047	-0.0187	0.0198	0.0198
20	5	-0.00.10	0.0011	6.0230	0.0230	20	6	0.0116	0.0033	0.0220	6.0226
20	7	-0.0179	-0.0069	0.0178	0.0179	20	8	0.0069	-0.0024	0.0244	0.0243
***	4	0.0284	-0.0077	0.0160	0.0162		10	-0.0013	0.0145	0.0228	
20	11	0.0230	0.0037	0.0182	9.0182		12				0.0228
20	13	0.0040	-0.0006	0.0223	0.0162			-0.0191	0.0080	0.0206	0.0204
23	13	0.0085	-0.0068	0.0220			14	0.6123	-0.0015	0.0198	0.0198
	17	-0.0016	0.0071	0.0228	0.0159		16	-0.0167	-0.0088	0.0200	0.0201
20	19	-0.0022	0.0006	0.6208	0.0202		18	-0.0096	-0.0187	0.0217	0.0196
20	.,	-0.0022	0.11006	0.0204	0.0208	20 :	20	0.0153	0.0644	0.0217	0.0218

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Table A.3: Fully Normalized Geopotential Coefficients Determined from 416 10° Mean Anomalies by Collocation. No Elevations Included. Noise Covariance Matrix D=0. a=6378140 m. Coefficients multiplied by 10° .

u	M	C	9	SIGMA	BICHA	M	H	c	8	SICMA	SICMA
,		-483.2466		0. 1293							
223	1	0.2343	0.0751	0.0945	8080.0	2	2	2.4441	-1.4526	9.0878	0.0868
3	-	0.7037		0.1927	0,0000		-				0.0000
3	1	1.7960	0.0687	0.2045	0.2093	3	2	1.1602	-0.4638	0.2102	0.2095
3	3	0.7672	1.5695	0.2095	0.2100						
4		1.0257		0.1117							
4	1	-0.4485	-0.3936	0.1078	0.1076	4	2	0.9340	0.4062	0.1070	0.1065
4	3	0.7718	-0.4191	0.10.33	0.1057	4	4	-0.2243	0.4157	0.1059	0.1061
5		0.2040		0.0732		_					-
3	1	-0.1577	-0.2423	0.0699	0.0699	5	3	0.3902	-0.1930	0.0695	0.0694
5 5	3	-0.2319	-0.1332	0.06.13	0.0681	5	4	-0.0862	-0.0181	6.0674	0.0677
9	5	-0.0014	-0.5070	0.0672	0.8691						
6	,	0.1246	9.0478	0.04.14	0.0292	6	2	0.2866	-0.3644	0.0288	6.0289
	3	-0.0162	-0.0618	0.0263	0.0259	6	4	-0.1792	-0.4151	0.0239	
6677777	5	-0.3680	-0.5424	0.02.7	0.0248	6	6	0.0017	-0.2346	0.0252	0.0248
7		0.2051	0.0929	0.0452	0.0240		•	0.0011	0.2340	0.0232	0.0237
÷	1	0.2026	0.0449	0.0412	0.0412	7	2	0.2928	0.1261	0.0411	0.0410
ż	3	0.1539	-0.1840	0.04:2	0.0399	7	4	-0.1626	-0.1636	0.0305	0.0389
7	5	0.0901	-0.0048	0.03114	0.0382	7	6	-0.3073	0.2070	0.0380	0.0384
7	7	-0.0293	-0.0949	0.0371	0.0391						
8		0.0619		0.0364							
11	1	-0.0443	0.0461	0.0307	0.0307	8	2	0.1292	0.0988	0.0308	0.0367
8	3	0.0812	-0.0213	0.0274	0.0294	8	4	-0.2115	0.0304	0.0281	0.0283
11	5	-0.0170	0.0339	0.0269	0.0272	8	6	-0.0877	0.1944	0.0269	0.0269
8	7	0.0404	0.0712	0.0269	0.0270	8	8	-0.1447	0.0915	0.0202	0.0282
9		0.1370		0.0315							
9	1	0.1813	-0.0271	0.0310	0.0310	9	2	0.1212	-0.0779	0.0310	0.0310
9	3	-0.1873	-0.0303	0.0373	0.0302	9	4	-0.0606	0.0354	0.0291	0.0291
9	7	-0.0582	-0.0317	0.02.11	0.0281	9	6	0.0922	9. 1884	0.0276	0.0271
9	4	-0.0836	-0.0199	0.02.4	0.0276	,	43	0.2044	0.0080	0.0276	0.0276
10	,	-0.0129 0.0483	0.0262	0.0206	0.02(H)						
10	1	0.1216	-0.0186	0.0234	0.0255	10	2	-0.0715	-0.0428	0.0256	0.0256
10	à	-0.0386	-0.0991	0.0216	0.0247	io	4	-0.0673	-0.1026	0.0236	0.0236
10	5	-0.0278	-0.0139	0.0221	0.0223	10	6	-0.0516	-0.0487	0.0216	0.0211
10	7	0.0064	-0.0170	0.0205	0.0209	10	ö	0.0441	-0.0371	0.0210	0.0211
10	9	0.1061	-0.0191	0.0210	0.0216	10	10	0.1077	-0.0314	0.0233	0.0224
11		-0.0929		0.0233							
11	1	-0.0222	0.0041	0.0278	0.0258	11	2	-0.0241	-0.0912	0.0258	0.0250
11	3	-0.0806	-0.1206	0.0231	0.0251	11	4	-0.1038	-0.0735	0.0240	0.0241
11	5	0.0152	0.6077	0.0229	0.0230	11	6	-0.0087	0.0093	0.0220	0.0217
11	7	0.0357	-0.1130	0.0212	0.0215	11	8	0.0073	0.0666	0.0209	0.0210
11	9	-0.0474	0.0833	0.0213	0.0217	11	10	-0.0295	0.0158	0.0223	0.0212
11	11	0.07911	-0.0171	0.02.14	0.0234						
12 12		0.04119		0.02/10			•	0 00/7	0 0000		
12	1	0.0183	-8.0914	0.0236	0.0255	12	2	0.0067	-0.0279	0.6257	0.0257
12	3	0.0129	0.0426	0.02:8	0.0248	12	6	-0.0673 0.0292	-0.0379	0.0241	0.0241
12	5	-0.0569	0.0320	0.0210	0.0214	12	å	0.0092	0.0315	0.0222 0.6208	0.0219
12	9	0.0139	0.0167	0.0298	0.0207	12	10	-0.9117	-0.0266	0.0215	0.0214
13	11	0.0990	0.0039	0.0217	0.0207	12	12	0.0141	-0.0100	0.0234	0.0235
13		0.0497	0.0039	0.0209	0.0211			0.0141	0.0100	0.0209	4.0233
13	1	-0.0042	0.0142	0.0274	0.0254	13	2	0.0077	-0.0381	0.0254	0.0254
13	3	-0.0195	0.0376	0.0216	0.0246	13	4	0.0048	-0.0059	0.0239	0.0239
13	5	0.0382	0.0403	0.02.10	0.0231	13	6	-0.0242	-0.0111	0.0220	0.0220
13	7	-0.0177	0.0132	0.0213	0.0214	13	8	-0.0238	0.0222	0.0206	0.0207
13	9	-0.0176	0.0325	0.0297	0.0201	13	10	0.0350	-0.0114	0.0207	0.0204
13	11	0.0065	0.0280	0.0213	0.0213	13	12	-0.0042	0.0994	0.6215	0.0217
13	13	-0.0379	0.0633	0.0243	0.0234						
1+		0.0125		0.02.4							

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14		0.0222	0.0077	0.0244	8.0244	14	2	-0.0426	-0.0187	0.0243	9.0248
14	3	0.0089	0.0050	0.02:14	0.0234	14	4	-0.0006	-0.0232	0.0226	0.0228
14	5	0.0141	-0.0087	0.0273	0.0219	14	6	-0.0051	0.0039	0.0210	8 9216
14	7	0.0316	-0.0149	0.0179	0.0199	14	a	-0.0301	-0.0200	0.0194	0.0194
14	9	0.0155	0.0437	0.01119	0.0100	14	10	0.0234	-0.0040	0.0191	6.0188
11	11	0.0327	-0.01135	0.0191	0.0190	14	12	0.0016	-0.0238	0.0199	0.0202
14	1:3	0.0382	0.0395	0.0273	0.0203	14	14	-0.0176	0.0132	0.0223	0.0223
15		-0.0020		0.0215							
15	1	0.0331	0.0000	0.02(0)	0.0248	15	2	0.0047	0.0(83	3.024.2	0.0342
15	3	0.0459	0.0463	0.0215	0.0236	15	4	0.0032	-5 0172	6.4229	6.0229
15	5	0.0095	0.0159	0.0221	0.0221	13	6	-0.0071	. 9269	0.0213	0.0213
15	7	0.0611	0.0147	0.0205	0.0205	15	B	-0.0427	0.0223	0.0197	0.0196
15	9	0.0026	-0.0038	0.0193	0.0194	15	10	-0.02/2	0.0000	0.0190	0.0189
13	11	-0.0061	0.01611	0.0193	0.0192	13	12	-0.0155	0.0697	0.0.94	0.0195
13	1:3	-0.0200	0.0173	0.0295	0.0203	15	14	0.0136	-0.0215	0.0207	0.0206
15	13	-0.0285	0.0996	0.0228	0.0223						
14		0.0294		0.0213							
16	1	-0.0009	0.0144	0.0214	0.0254	16	4	-0.0090	0.0008	9 0236	0.0236
16	3	-0.0236	0.0212	0.0237	0.0238	16	4	0.0350	0.06111	6.0228	0.0228
16	5	-0.0113	0.0219	0.0222	0.0222	16	6	0.0003	-0.0307	6.0215	0.0215
16	7	-0.0160	-0.0078	0.0207	0.0208	16	a	-0.0517	0.0340	0.0201	0.0200
16	9	-0.0037	-0.0393	4410.0	0.0193	16	10	-0.0025	-0.0115	0.0194	0.0193
10	11	0.0074	-0.0126	0.0172	0.0188	16	12	0.0190	-0.0011	0.0195	0.0193
14	13	0.0000	0.0160	0.0201	0.0193	16	14	-0.0046	-0.0248	0.0207	0.0206
16	15	-0.0111	-0.0350	0.0213	0.0203	16	16	-0.0179	-0.01119	0.6228	0.0228
17		0.0029		0.0173							
17	1	0.0064	0.0281	0.0237	0.0267	17	2	-0.0422	0.0199	0.0200	0.0200
17	3	0.0081	-0.0186	0.0214	0.0255	17	4	-0.0195	0.0282	9.0214	0.0214
17	5	-0.0184	0.0109	0.0228	0.0220	17	6	-0.0230	-0.9373	0.0212	0.0212
17	7	0.0223	-0.0230	0.0211	0.0211	17	8	0.0219	-0.0113	0.0201	0.0201
17	9	-0.0202	-0.0377	0.0116	0.0199	17	10	-0.0162	0.0155	0.0193	0.0193
17	11	0.0003	0.0029	0.0195	0.0190	17	12	-0.0168	0.0015	6.0191	0.0190
17	13	0.0191	0.0111	0.02 18	0.0184	17	14	-0.0120	0.0201	0.0198	0.0199
17	15	0.0167	0.0181	0.0223	0.0192	17	16	-0.0118	0.0139	0.0210	0.0210
17	17	-0.0321	0.0069	0.0228	0.6227						
181		0.0102		0.0300							
181	1	-0.0251	-0.0419	0.0138	0.0138	18	2	-0.0057	0.0033	8.0308	0.0308
183	3	-0.0093	-0.0084	0.0119	0.0120	18	4	0.00113	0.0069	0.0286	0.0206
111	5	0.0032	0.0156	0.0140	0.0160	10	6	0.0199	-0.0010	0.0244	0.0244
181	7	-0.00++	-0.0023	0.0110	0.0191	18	8	0.0298	-0.0058	6.0211	0.0211
111	9	0.0071	0.0099	0.0172	0.0194	18	10	0.0246	-0.0052	0.0195	0.0195
111	11	-0.0234	-0.6098	0.0193	0.0189	18	12	0.0011	-0.0179	6.0193	0.0191
111	13	-0.0066	-0.0554	0.0214	0.0165	18	14	0.0003	-0.0205	0.0197	0.0197
111	13	-0.0442	-0.0291	0.6228	0.0163	1/1	16	0.0113	0.0123	0.0200	6.0207
115	17	0.0092	-0.0110	0.0210	0.02011	181	113	-0.0046	-0.0122	0.0290	0.0131
19		-0.0002		0.0250							
1.3	1	0.0013	0.0221	0.02.15	0.0203	19	2	0.0229	-0.0107	0.0244	0.0244
19	:3	0.0023	-0.0168	0.02 19	0.0229	19	4	0.0174	-0.0095	0.0182	0.0182
1.1	5	-0.0093	0.0034	0.02 %	0.0266	19	6	0.0041	0.0157	0.0134	0.0134
19	7	-0.0015	0.0064	0.0234	0.0254	19	a	0.0230	-0.0004	0.0162	0.0162
19	9	0.0029	0.0056	0.0213	0.0217	19	10	-0.0166	-0.0116	0.01113	6.0182
19	11	0.0003	0.0092	0.0195	0.0194	19	12	-0.0011	-0.00311	0.01119	0.01117
19	13	0.0097	-0.0268	0.02 23	0.0131	19	14	0.0164	-0.0063	0.0190	0.0190
19	15	0.0030	-0.0150	0.0236	0.0146	19	16	-0.0254	0.0094	0.0198	0.0190
19	17	0.0193	-0.0076	0.02.4	0.0208	19	143	0.0363	-0.0091	0.0225	0.01811
13	10	0.01911	0.0100	0.02:1	0.0221						
20		-0.0056		0.0232							
20	1	-0.0138	-0.0052	0.0210	0.0210	20	2	-A.0054	0.0041	0.0223	0.0223
20	3	-0.0100	0.0076	0.0210	0.0230	20	4	-0.0033	-0.01911	0.0186	0.01116
****	5	-0.0043	0.0009	0.0226	0.0226	20	6	0.0136	0.0441	0.0214	0.0213
20	7	-0.0182	-0.0009	0.0193	6.0163	20	8	6.0063	-0.0010	0.0242	0.0242
20	9	0.0293	-0.0094	0.0112	0.0143	20	10	0.0013	0.01711	0.0219	0.0219
20	11	0.0240	0.0018	0.0170	0.0170	20	12	-0.0199	0.0098	0.0196	0.0194
20000	13	0.0033	-0.0023	0.0219	0.0139	20	14	0.0135	-0.0016	0.0100	0.01119
20	13	0.0098	-0.0093	0.02.4	0.0144	20	16	-0.0104	-0.0092	0.0193	0.0194
20	17	-0.0014	0.0074	0.0195	0.0193	20	111	-0.0110	-0.0204	0.0214	0.0190
20	19	-0.0026	0.0002	0.0203	0.0203	20	20	0.0175	0.0045	0.0214	0.0215

Table A.4: Fully Normalized Geopotential Coefficients Determined from 416 10° Mean Anomalies by Integration. All coefficients multiplied by 10° . (Error Estimates not corrected by β_n^{-1} .)

N	H	C	8	SICMA	SICMA	N	H	c	8	BICMA	SICHA
		-403.5679		0. 14:15							
400000	1	0.2284	0.0726	0.1841	0.1898	2	2	2.4380	-1.4532	0. 1450	0.1461
3		0.5031		0.0862			-				-
3	3	0.7935	1.6197	0.0696	0.0965	3	2	1.1970	-0.4740	0.0876	0.01150
3	3	0.6038	1.0197	0.0600	0.0701						
4	1	-0.4561	-0.3934	0.0594	0.0593		2	0.3324	0.4237	0.0616	0.0634
4	3	0.7911	-0.4269	0.0521	0.0547	4	2	-0.2285	0.4259	0.0464	0.0438
0		0.1559		0.0437		113					
5 5	1	-0.1387	-0.274H	0.0436	0.0423	5	2	0.4009	-0.1949	0.0461	0.0453
2	3	-0.2318	-0.1319	0.6446	0.6445	5	4	-0.0861	-0.0195	0.0379	0.0372
6	5	0.1026	-0.5222	0.0325	0.0334						
	1	0.1204	0.0476	0.0334	0.0343	6	2	0.2723	-0.3512	9.0350	0.0342
6	3	-0.0105	-0.0597	0.0364	9.9361	6	4	-0.1776	-0.4002	0.0338	6.0333
6	5	-0.3573	-0.5234	0.0270	0.0298	6	6	0.0066	-0.2309	0.0256	0.0259
7		6. 1833		0.0274							
7	1	0.1994	0.0313	0.0297	0.0298	7	2	0.2866	0.1244	0.0271	0.0276
7	3	0.1613	-9.1813	0.0293	9. 0295	7		-0.1629	-0.1626	0.0293	0.0209
77777	5	-0.0312	-0.0039	0.0210	0.0271	7	6	-0.3065	0.2026	0.0228	0.0224
à		0.0152	-0.0704	9.0236	0.0207						
B	1	-0.0433	0.0461	0.0244	0.0241	8	2	0.1178	0.0995	0.0237	8.0246
u	3	0.0838	-0.01" 1	0.0233	0.0231	8	4	-0.2054	0.0526	0.0257	0.0247
11	6	-0.9156	0.0338	6.0230	0.0342	8	6	-0.0826	0.1837	0.0212	0.0213
t.	7	0.0396	0.0659	0.0188	0.0103	0	0	-0.1370	0.0909	0.0182	6.0168
4		0, 1200		0.0202							_
9	1	6. 1729	-0.03110	0.0207	0.0206	9	2	0.1191	-0.0779	0.0204	0.0210
9	3	-0.1768	-0.0294	0.0201	0.0201	9	6	-6.03110	0.0524	0.0209	0.6200
9	7	-0.0560	-0.0279	0,0209	0.0221	9	B	0.0071	0.0102	0.0194	0.0194
9	9	-0.0175	0.6203	0.0151	0.0148			V. 1700	0.0102	0.0137	0.0132
10		0.0210	0.0200	0.0171							
10	1	0.1146	-0.0170	0.0160	0.0183	10	2	-0.0713	-0.0372	0.0176	0.0178
10	3	-0.0330	-0.0946	8.0177	0.0178	10		-0.0593	-0.0936	0.0177	0.0171
19	5	-0.0241	-0.0129	0.0178	0.0186	10	6	-0.0521	-0.0476	0.0183	0.0103
10	7	0.0787	-0.0149	0.0161	0.0161	10	10	0.0445	-0.0525 -0.0315	0.0153	6.0145
11	,	-0.0963	-0.0203	0.0158	W. 0130	10	10	0.1135	-0.0.113	6.0126	0.0132
ii	1	-0.0276	-0.0030	0.0149	0.0150	11	2	-0.0233	-0.0882	0.0161	0.0163
ii	3	-0.0729	-0.1145	0.0151	0.0149	11	4	-0.0983	-0.0003	0.0159	0.0154
11	5	0.0135	0.0071	0.6131	0.0155	11	6	-0.0115	0.0052	0.0162	0.0160
11	7	0.0358	-0.1069	0.0156	0.0154	11	n	0.0079	0.0614	0.0139	0.0133
11	9	-0.0478	0.0771	0.0131	0.0123	11	10	-0.0216	0.0163	0.0116	0.0114
11	11	0.0703	-0.0127	0.0113	0.0113						
13		-0.0305	-0.0296	0.0142	0.0131	12	2	0.0015	-0.0231	0.0138	0.0145
12	3	0.0149	0.0395	0.0136	0.0136	12	-	-0.0639	-0.0334	0.0133	0.0132
12	6	0.0544	-0.0016	0.0136	0.0142	12	6	0.0237	0.0461	0.0137	0.0135
12	7	-0.0230	0.0310	0.0144	0.0141	12	ü	0.0107	0.0244	0.0135	0.0128
12	9	0.0139	0.0162	0.0110	0.0113	12	10	-0.0072	-0.0251	0.0111	0.0111
12	11	0.0003	0.0047	0.0009	0.0101	12	12	0.0137	-0.00111	0.0101	0.0090
13		0.0461	**	0.0122							_
13		-0.6098	0.0033	0.0115	0.0121	13	2	0.0078	-0.03119	0.0116	0.0124
10	3	-0.0145	0.0359	0.0126	0.0124	13	4	0.0042	-0.0044	0.0117	0.0114
13	5	-0.0173	0.0408	0.0119	0.0121	13	8	-0.0222	0.0107	0.0123	0.0123
13	6	-0.0173	0.0302	0.0113	0.0111	13	10	0.0315	-0.0078	0.0129	0.0122
13	11	0.0029	0.0270	0.0096	0.0098	13	12	-0.6041	0.0925	0.0007	0.0089
iä	ià	-0.0374	0.0626	0.0006	0.0096		-				3.0007
14		0.8027		0.0104	3.5.5.7/6.5						

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14	1	0.0223	0.0101	0.0106	0.0113	14 2	-0.0476		0.0163	0.0102
14	3	0.0123	0.0023	0.0114	0.0111	14 6	-0.0019		0.0107	0.9103
14	2	0.0159	-0.0101	0.0103	0.0105		-0.0004		6.0100	0.0110
14	7	0.0274	-0.0132	0.0109	0.0108	14 8			0.0111	0.0106
14		0.0162	0.0394	0.0111	0.0108	14 16			0.0097	6. 8094
14	11	0.0289	-0.0766	0.0009	6.00BB	14 12			6.0004	9.00117
14	13	0.0074	0.0240	0.0076	0.0078	14 14	-0.0108	0.0105	0.0075	0.6086
13		-0.0047 0.0203	0.0243	0.0049	0.0994	15 2	0.0053	0.0100	0.0096	0.0009
13	3	6.0407	0.0477	0.0093	6.0004		0.0037		6.6193	3.0099
15	5	0.0096	0.0144	0.0007	w. 0090	15		-0.0251	0.0005	3.0000
15	7	0.0575	0.0128	0.0008	9.6097	13 (U.0079	0.0094
15	•	0.0053	-6.0065	0.0097	0.0097	15 16			e. 0095	0.0093
15	11	-0.00-2	0.0146	0.0003	0.0001	15 13			0.0078	0.0078
15	13	-0.0215	0.0.04	0.0074	0.0077	15 14			0.006B	0.0069
15	13	-0.6242	0.0102	0.0067	0.0071				4.0000	•
14		0.0201		0. 6099						
10	1	-0.0098	0.0187	0.0067	6.0071	16 2	-0.0138	0.0014	0.0094	0.0095
16	3	-0.0215	0.0213	0.0079	0.0077	16 4			0.0091	0.0040
96	3	-0.0097	0.0204	0.0083	0.0004	16 6			0.0079	0.0082
16	7	-0.0107	-0.0072	0.0089	0.00119	16 8	-0.0537		4.88BB	0.0085
16	9	-0.0017	-0.0580	0.0005	6.00BB	16 16		-0.0091	0.0087	0.0007
16	11	0.00114	-0.0150	CH00.0	0.0002	16 12	2 0.0172	-0.0044	0.0073	9.0069
16	13	-0.0001	0.0140	0.0066	0.0U72	16 14		-0.0253	6.8066	9.0667
16	15	-0.0116	-0.0367	0.0059	0.0063	16 16	-0.0225	-0.0170	0.0065	0.0059
17		0.0031		0.0090	2 27 27					
17	1	0.0007	0.6262	0.0059	0.0062	17 2			0.000	0.0081
17	3	0.0168	-0.0226	6.0077	0.0075	17 4			0.0073	6.0372
17	6	-0.0204	0.0126	0.0000	6.0003	17 6			0.0067	6.0071
17	7	0.0235	-0.0245	0.0076	0.0077	17 8		-0.0147	0.0082	●.0078
17	9	-0.0191	-0.0365	0.0074	e.007U	17 10			0.0077	0.007A
17	11	-0.0018	0.0063	0.0077	0.0076	17 12			0.0072	0.0070
17	13	0.0171	0.0117	0.0034	0.0069	17 14			0.0061	0.0862
17	13	0.0191	6.0102	0.0034	0.0064	17 16	-0.6097	0.0151	0.0054	0.0654
14	11	-0.0360	0.00711	0.0056	0.0054					
111		-0.0122	-0.031111	0.0038	0.0090	18 2	-0.0112	9. 9036	0.0024	0.0025
in	:	-0.0091	-0.0129	0.0092	0.0091	10		0.0004	0.0042	0.0023
111	5	0.0000	0.0177	0.0078	0.0002	10 6	0.0212	-0.0025	0.0062	0.0044
ia	7	-0.0048	-0.0022	0.0063	8.0063	in			0.0073	8.0076
113	•	0.0099	0.0114	0.0000	0.0073	10 10		-0.0047	0.006B	0.0068
14	11	-0.0192	-0.0127	0.0071	0.0069	10 12		-0.0221	0.0067	6.0067
111	13	-0.0093	-0.0360	0.0040	0.0073	18 14		-0.0223	0.0054	8.0055
111	15	-0.0470	-0.0381	0.0045	0.0063	10 10		0.0098	9.9056	0.0049
10	17	0.0073	-0.0103	0.0036	6.8045	18 16			0.0024	0.0065
19		0.0001		0.0041	•,•••					
19	1	-0.0062	0.0267	0.0073	0.0075	19 :	0.0372	-0.0176	0.0044	0.0044
19	3	0.0038	-0.0275	0.0064	0.0063	19 4	0.0254	-0.0172	0.0078	0.0069
19	5	-0.0114	0.0066	0.0037	0.0039	19 6			0.0077	0.0078
19	7	0.0001	0.0031	0.0041	0.0043	19 4	0.0261	-0.0011	0.0067	0.0065
19	9	0.0047	0.0063	0.0061	0.0063	19 16		-0.0152	0.0062	0.0063
19	11	0.0028	0.0098	0.0061	0.0061	19 13			0.0063	0.0062
19	13	0.0104	-0.0292	0.0039	0.0074	19 14	0.0206	-0.0018	0.0053	0.0054
19	15	0.0000	-0.01711	0.0034	0.0058	19 16			0.0053	0.0045
14	17	0.0240	-0.0095	0.6049	0.0043	19 18	0.0427	-0.0127	0.0039	0.0046
19	19	0.0323	9.0142	0.0043	0.0045					
20		-0.0117		0.0040						
20	1	-0.0275	-0.0072	0.0037	0.0050	20 :		0.0030	0.0053	0.0053
20	3	-0.0166	0.0132	0.0043	0.0042		-0.0127	-0.0349	0.0069	0.0068
20	5	-0.0053	0.0008	0.0039	0.0041	20 6		0.0052	0.0054	0.0055
20	7	-0.0274	-0.0137	0.6963	0.8864	26 8			0.0032	6.0033
20	9	0.0395	-0.0134	0.0063	0.0066	20 10	-0.0006	0.0233	0.0052	0.0053
20		0.0342	0.0007	0.0036	0.0057	20 12			0.8054	0.0055
20	13	0.0033	-0.0060	0.0033	0.0071	20 14			0.6052	0.0050
20	15	0.0149	-0.0177	0.0033	9.0036	20 16		-0.8174	0.0042	0.0043
20	17	-0.0033	0.0003	0.0046	0.0041	20 11		-0.0225	0.0038	6.0043
20		-0.0033	0.0003	0.0036	0.6039	20 26	0.0262	0.0052	0.0042	0.0036

